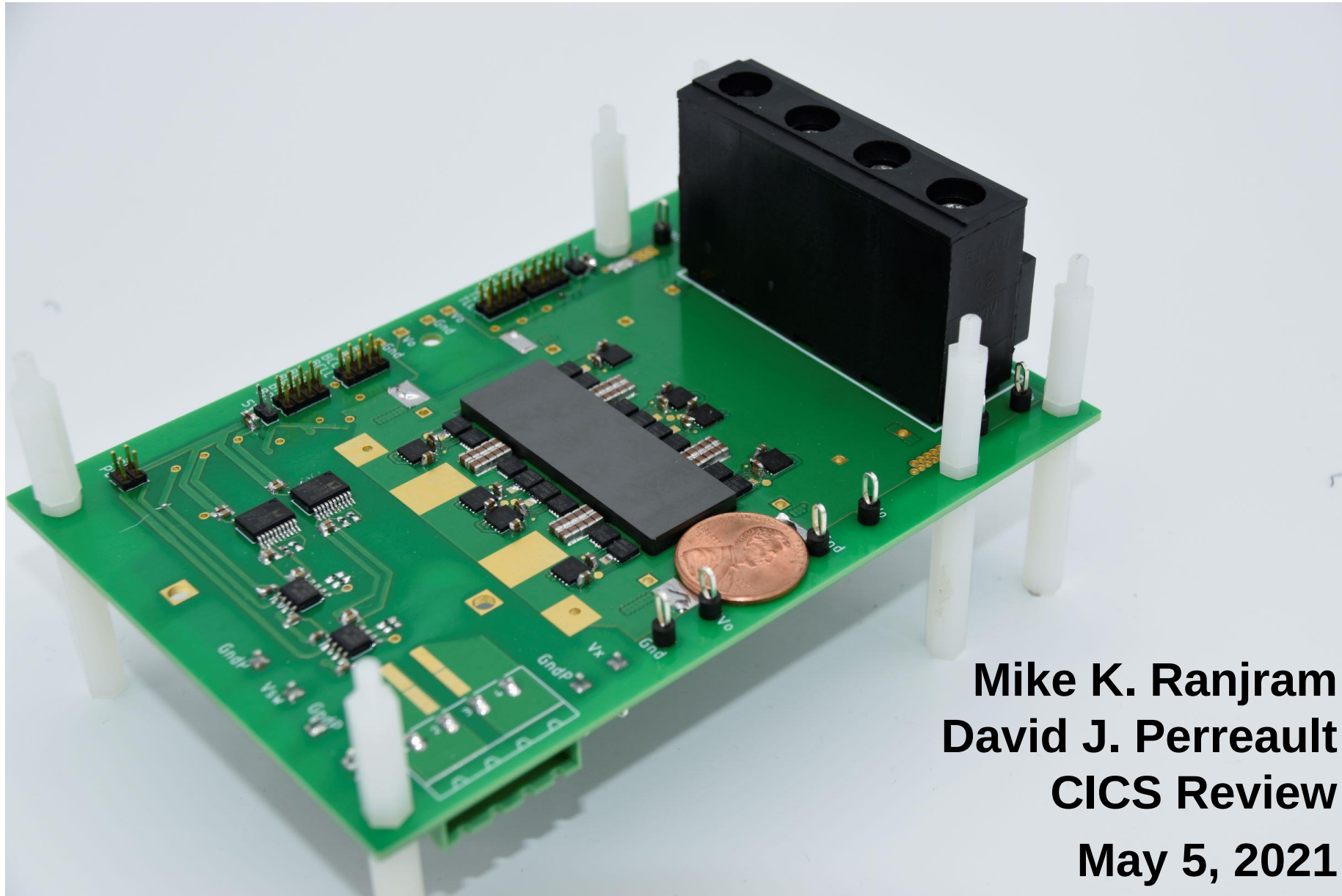
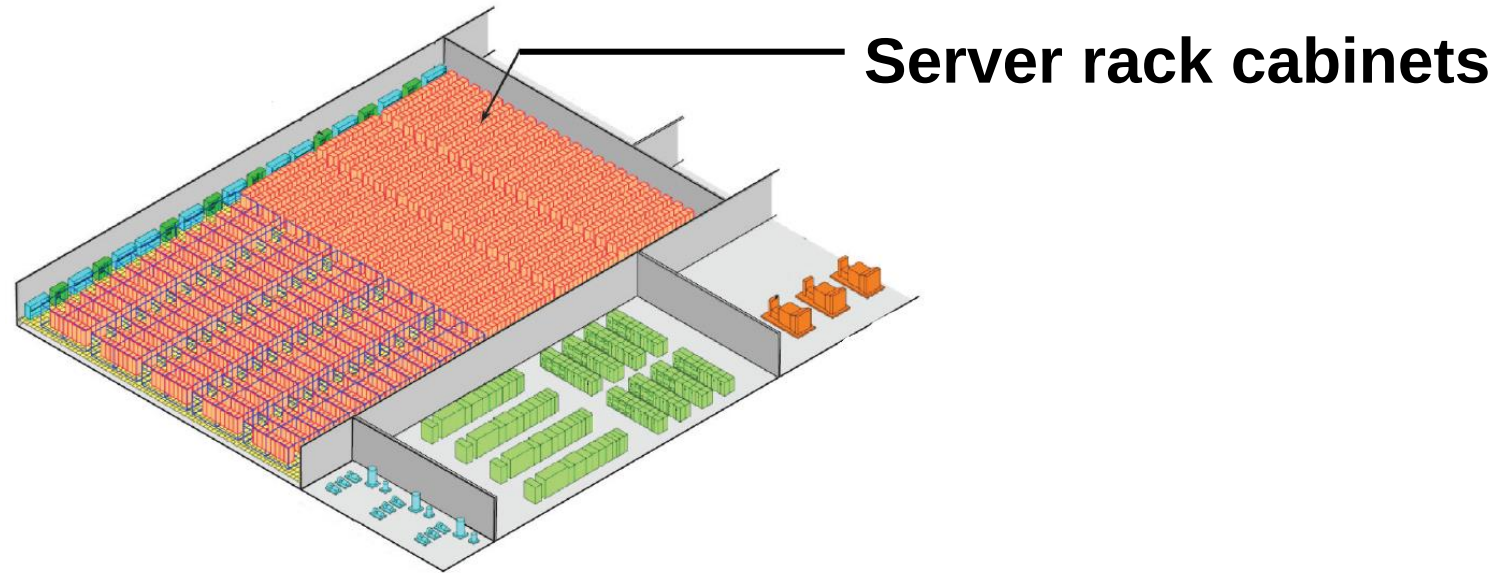


A Miniaturized Data Center Power Supply Using a Split-Phase, Fractional Turn Transformer



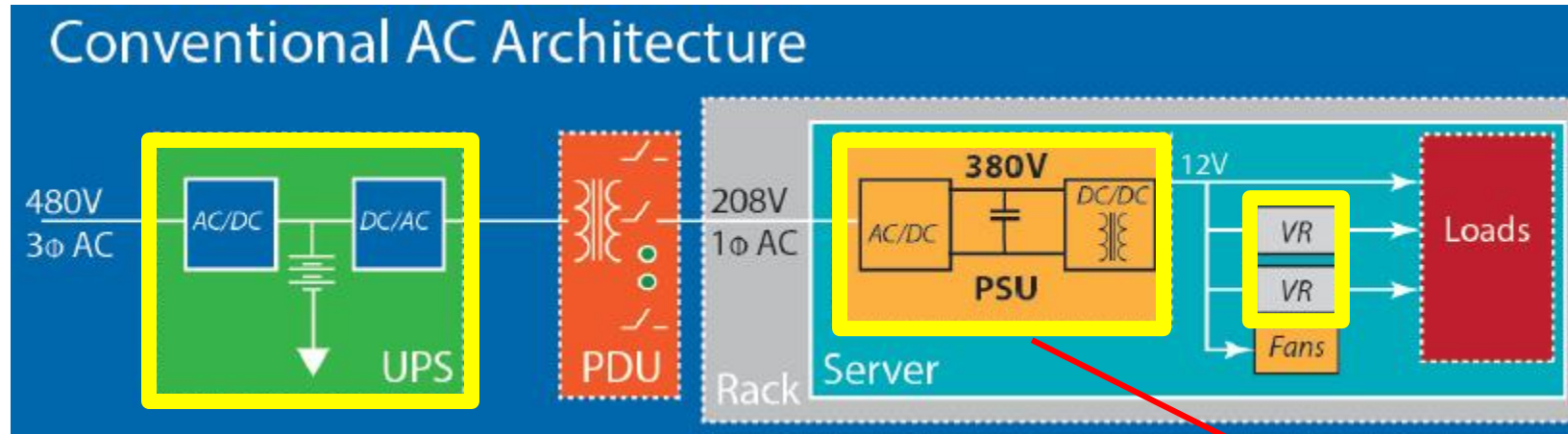
Mike K. Ranjram
David J. Perreault
CICS Review
May 5, 2021

Data Centers Are An Important and Growing Load



- Much of our virtual world “lives” in data centers
- Represent ~2% of total US electrical energy consumption
 - ~ Total solar PV energy produced in 2019

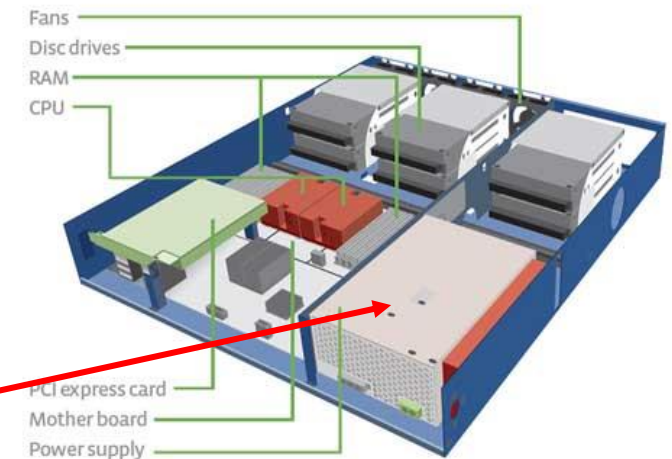
Data Centers Rely on Many Power Electronic Converters



- 75% eff. typical (converters *only*)
- Much lower if cooling power included

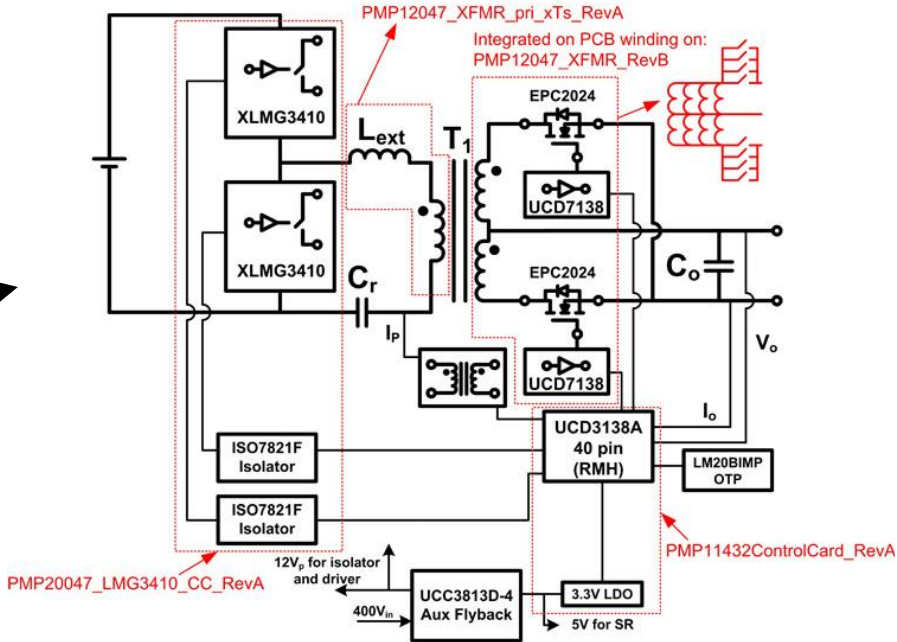
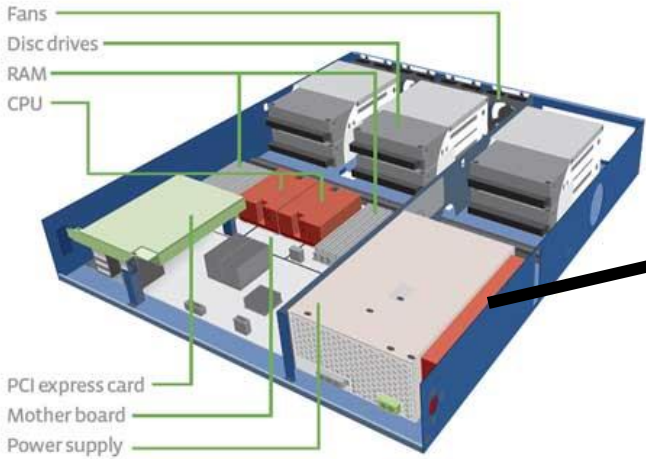
■ On server level, power supply miniaturization especially important

Open Compute Project Server



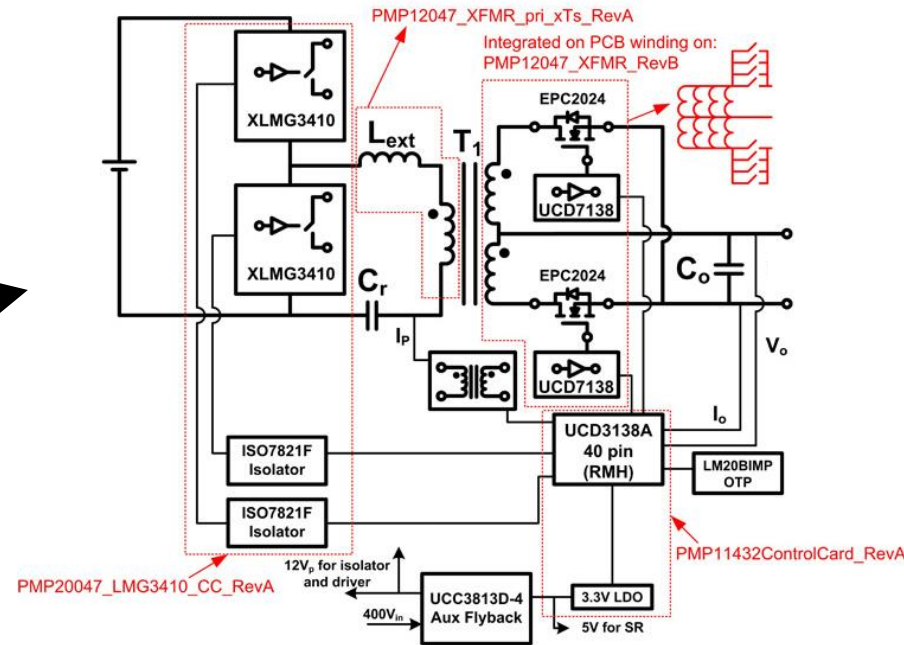
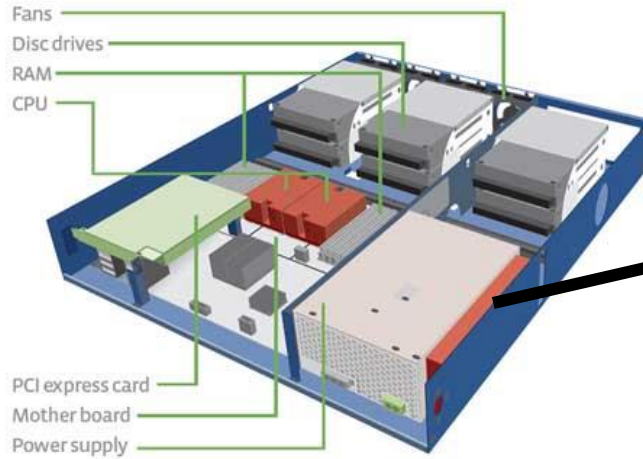
What Does This Supply Look Like Schematically?

Open Compute Project Server



Three Conversion Steps, but the Transformer Does the Most

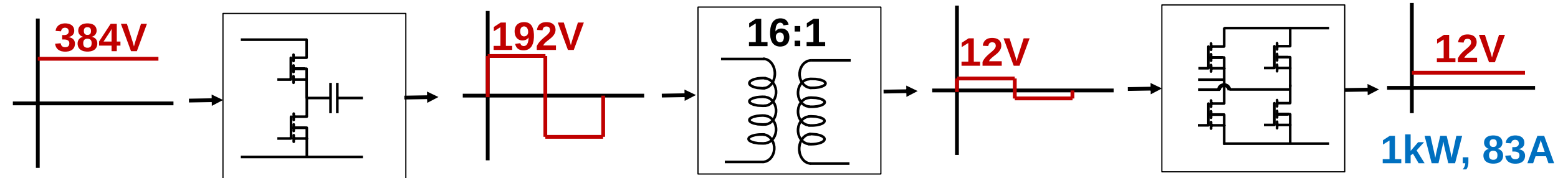
Open Compute Project Server



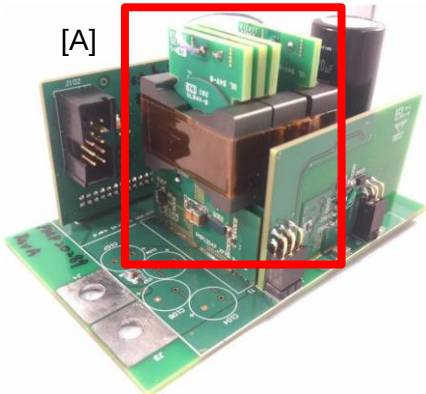
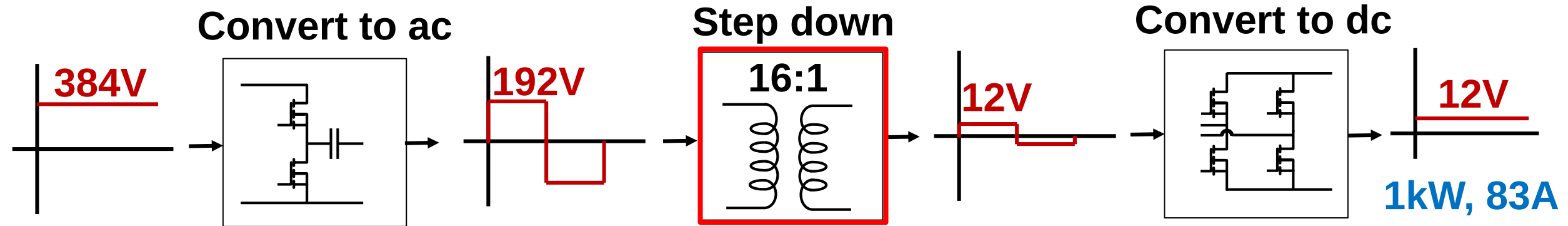
Convert to ac

Step down

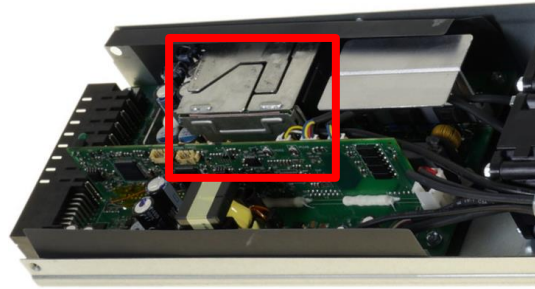
Convert to dc



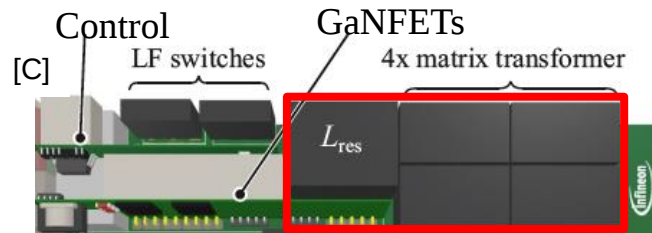
High Step-Down, High Current Transformer is a Critical Bottleneck



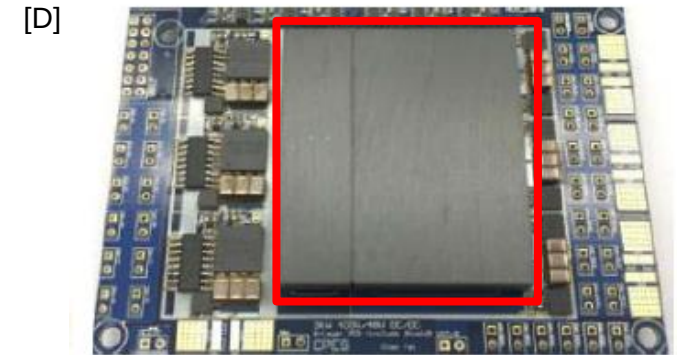
12V/500W



12V/1kW



12V/3kW



48V/3kW

[A] <https://www.ti.com/tool/PMP20289>

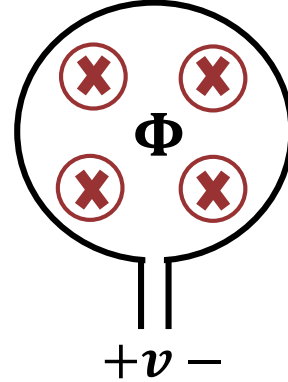
[B] <https://benchmarking.ihsmarkit.com/550162/teardown-delta-dps-1600ab-4-a-psu>

[C] M. Kasper, D. Bortis, J. W. Kolar and G. Deboy, "Hyper-efficient (98%) and super-compact (3.3kW/dm3) isolated AC/DC telecom power supply module based on multi-cell converter approach," 2014 IEEE Energy Conversion Congress and Exposition (ECCE), Pittsburgh, PA, 2014, pp. 150-157

[D] C. Fei, R. Gadelrab, Q. Li and F. C. Lee, "High-Frequency Three-Phase Interleaved LLC Resonant Converter With GaN Devices and Integrated Planar Magnetics," in IEEE Journal of Emerging and Selected Topics in Power Electronics, vol. 7, no. 2, pp. 653-663, June 2019.

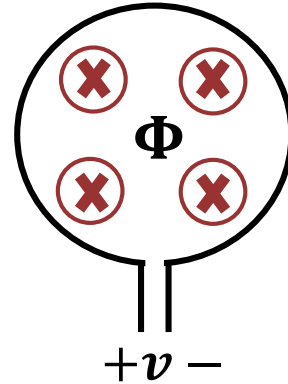
Review: Transformer Operating Principle

■ $\frac{d\Phi}{dt} = \frac{v}{N}$ (sign by Lenz's Law)



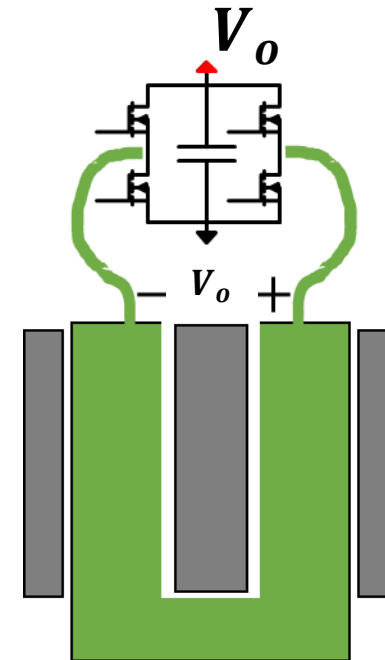
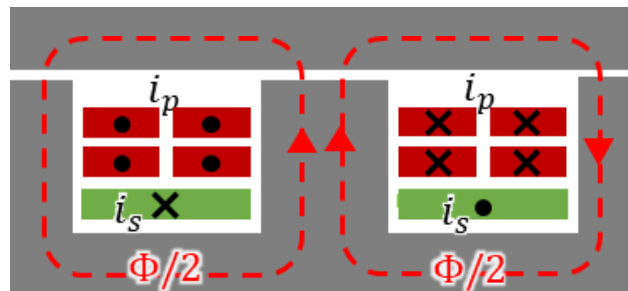
Review: Transformer Operating Principle

■ $\frac{d\Phi}{dt} = \frac{v}{N}$ (sign by Lenz's Law)



■ $\frac{v_p}{N_p} = \frac{v_s}{N_s} \Rightarrow v_p : v_s = N_p : N_s$

e.g. $N_p : N_s = 4 : 1$

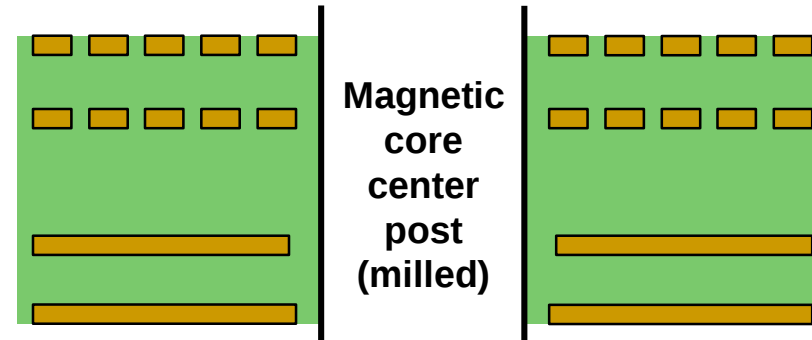


Planar Transformers Use PCB Windings

- Windings of inductors/transformers implemented as copper traces on printed circuit boards (PCBs)



Fig. 1. Planar transformer.



Planar Magnetics are Cheap, Easy to Build, with Great Thermals

- Low profile (minimize box volume)
- Good thermal characteristics (high surface area to volume)
- Ease of manufacturability
- Highly repeatable
- Lower cost than wire-wound alternatives

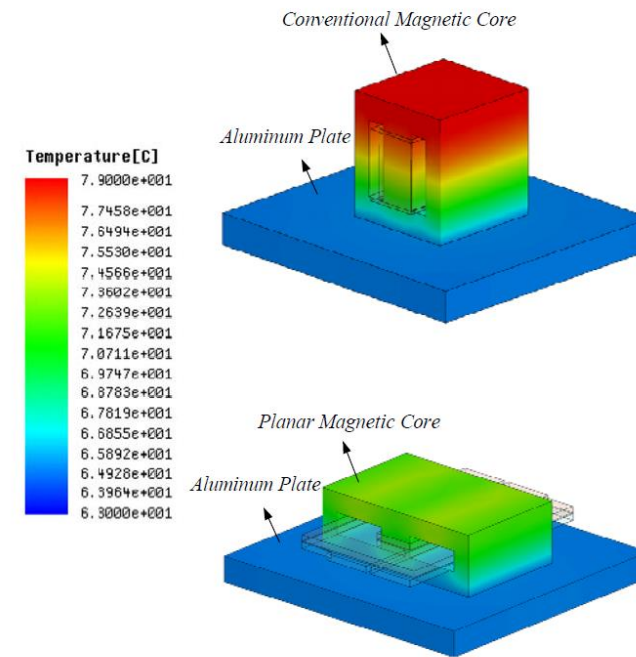
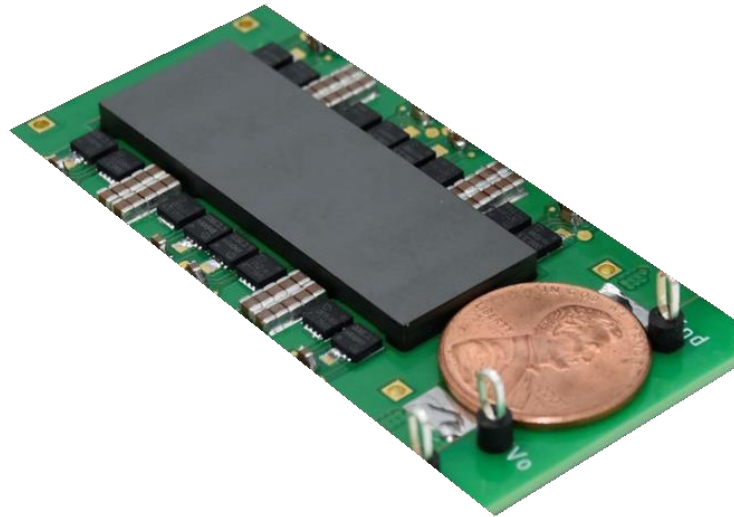
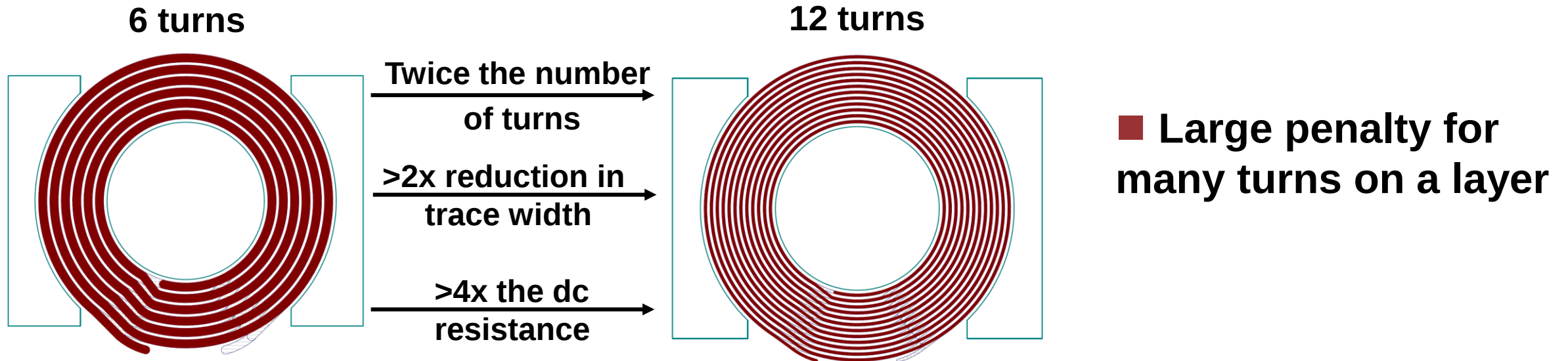
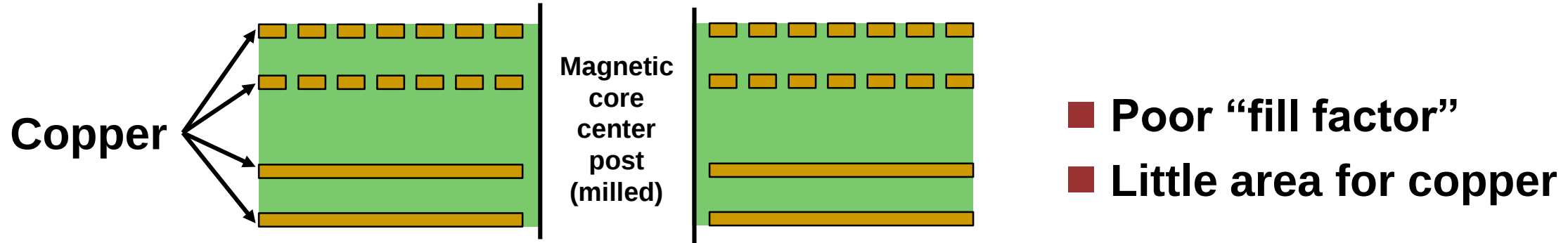
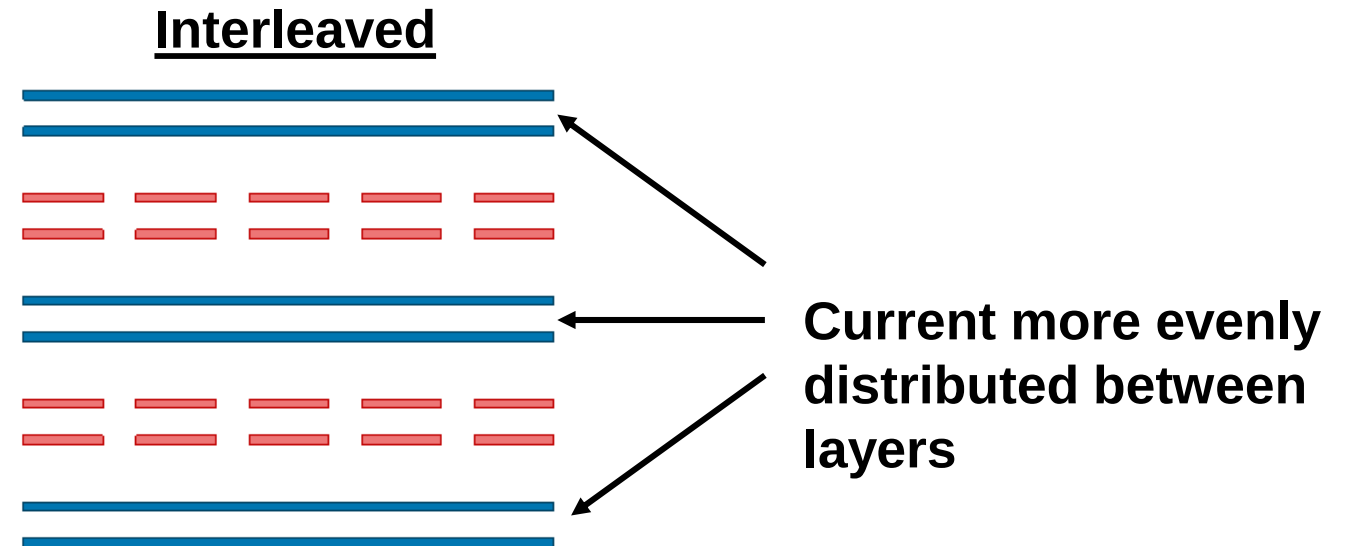
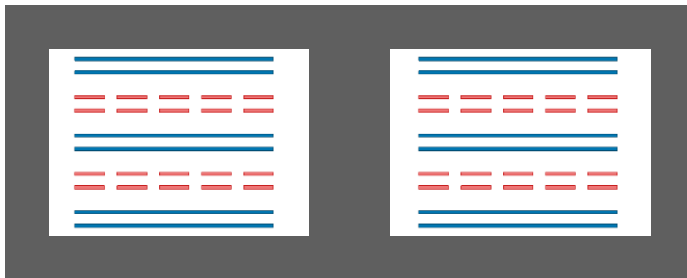
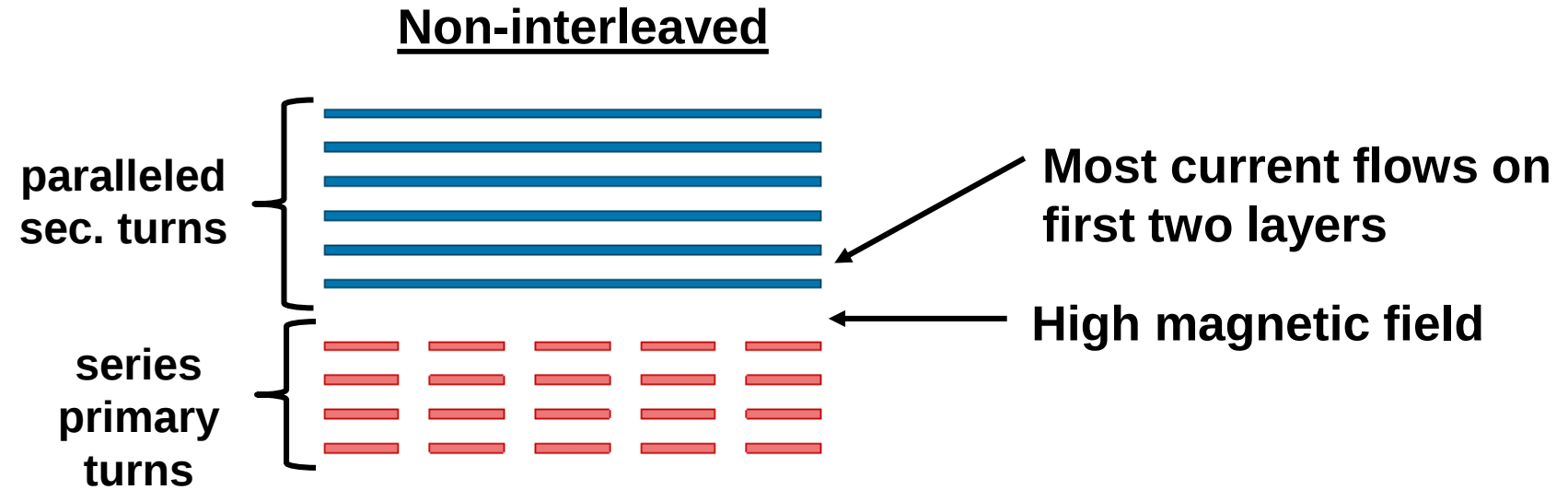


Fig. 1. Comparison of thermal behavior between conventional core and planar core.

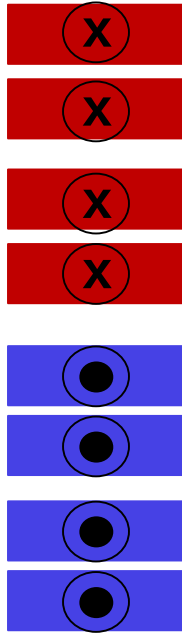
Many Turns and High Currents are Difficult in Planar Transformers



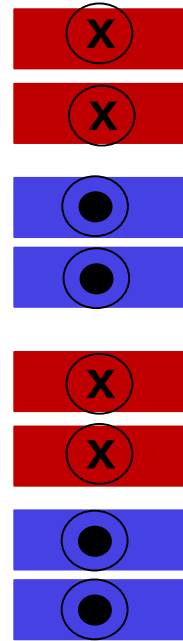
It Can Also Be Difficult to Use Additional Layers



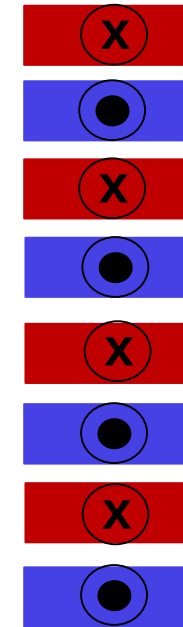
Resistance vs. Capacitance Trade-off of Interleaving



Not interleaved



Interleaved

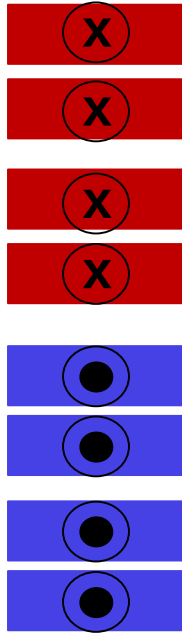


Ideally interleaved

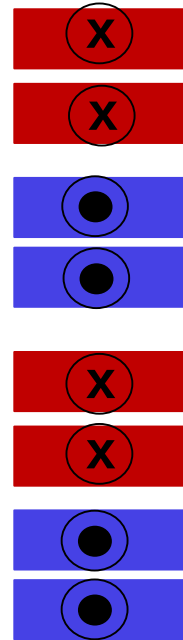
ac resistance  lower

capacitance  higher

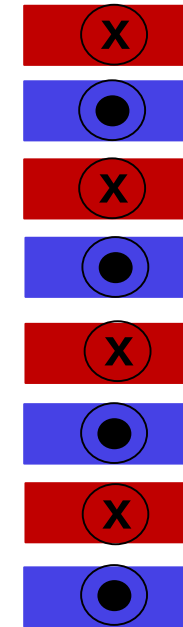
Resistance vs. Capacitance Trade-off of Interleaving



Not interleaved



Interleaved

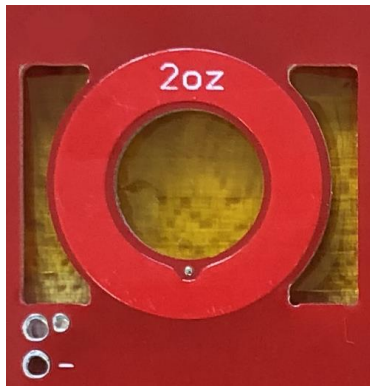
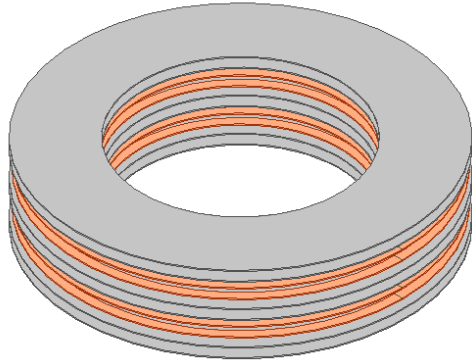


Ideally interleaved

ac resistance	→	lower
capacitance	→	higher
termination loss	→	Much higher

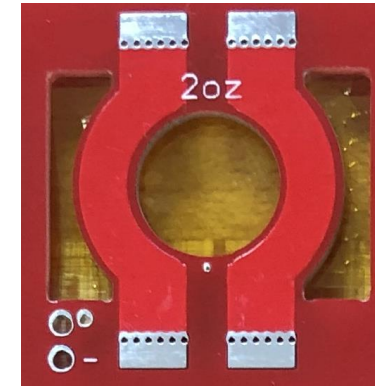
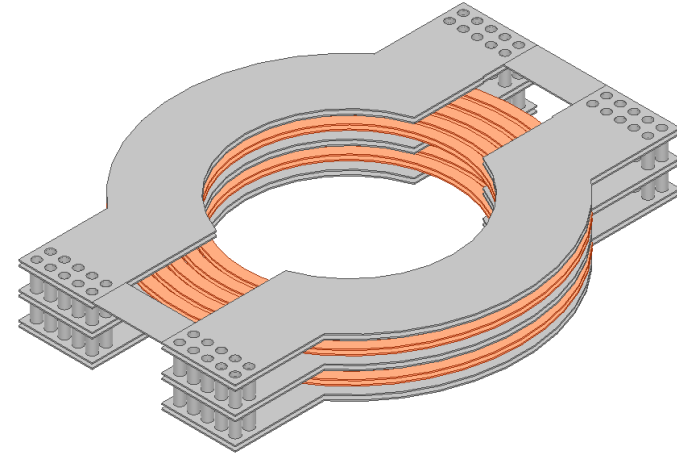
With Realistic Terminations, Loss Can Be Much Higher Than Expected

Ideal, perfectly terminated



0.29Ω

Practically terminated

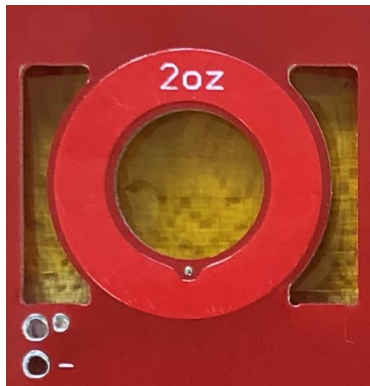
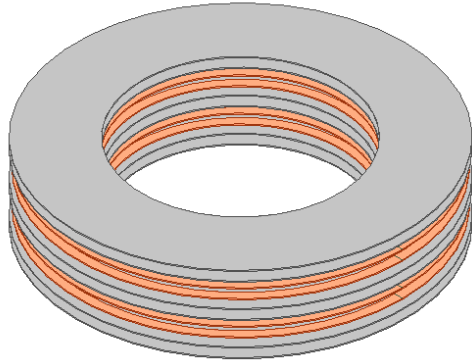


0.73Ω

Key: **Avoid complex vertical stack-ups** in this application space

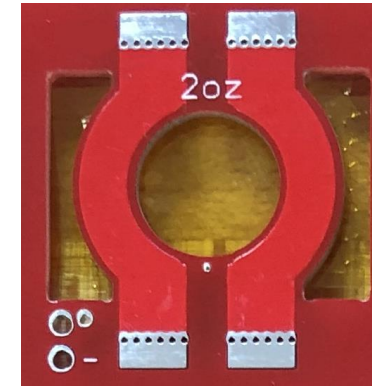
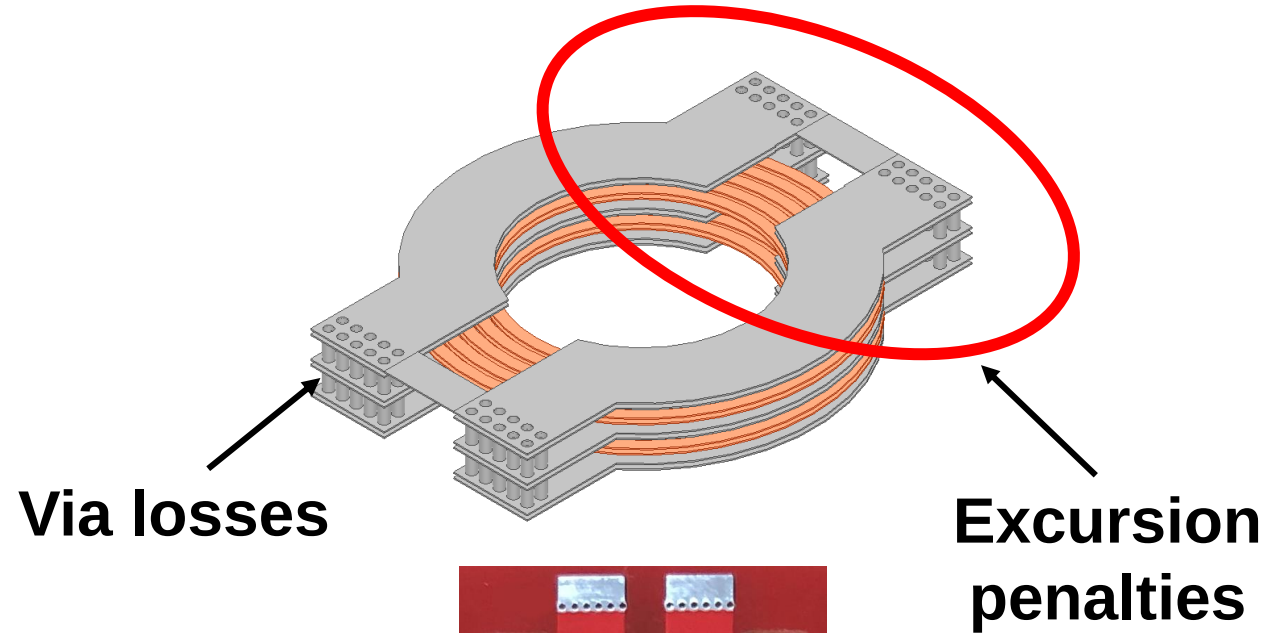
With Realistic Terminations, Loss Can Be Much Higher Than Expected

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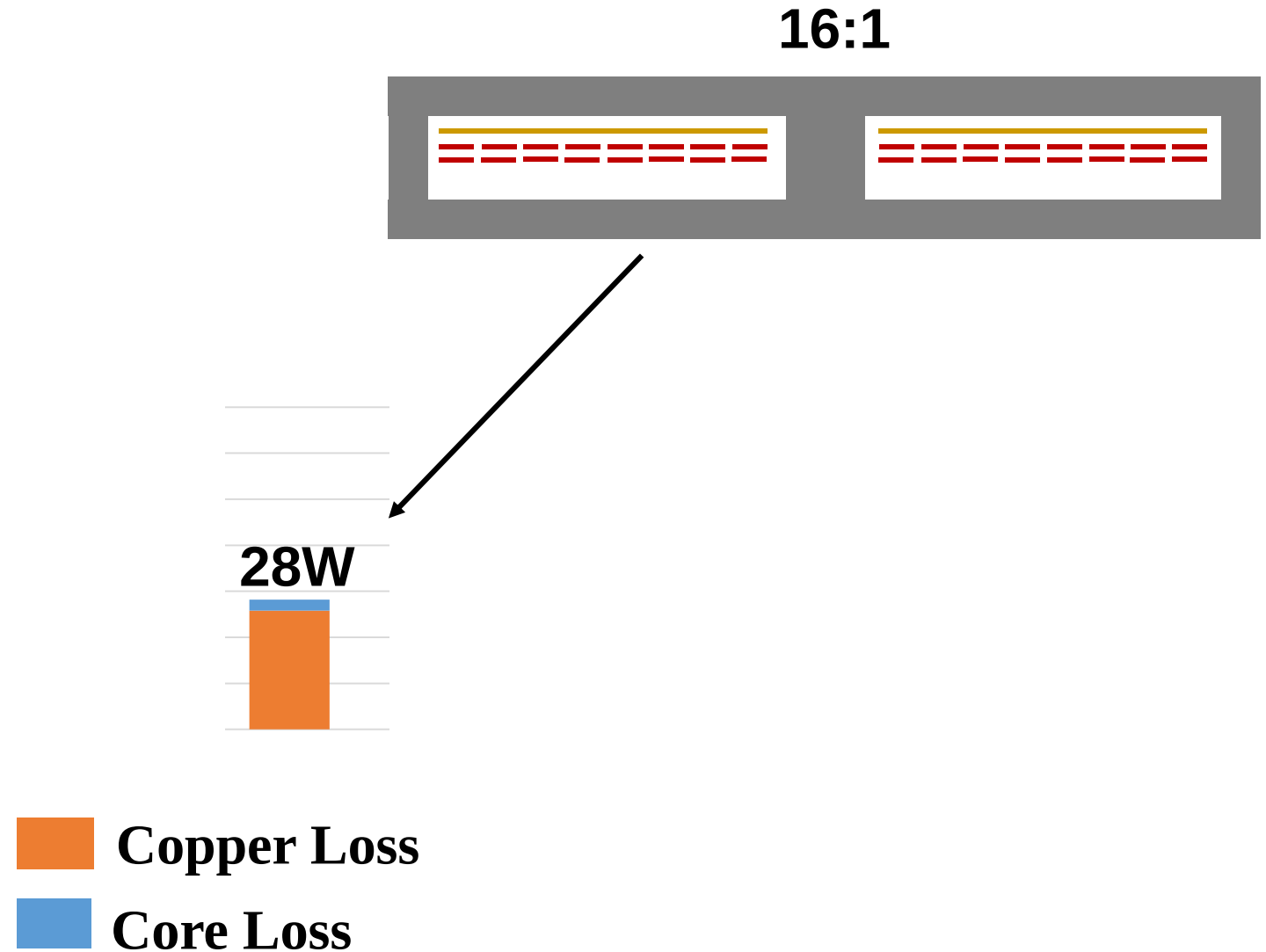
Practically terminated



0.73Ω

Key: **Avoid complex vertical stack-ups** in this application space

Minimizing Turns Count is Greatly Advantageous

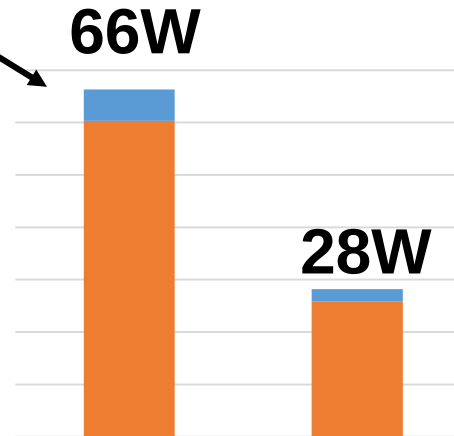
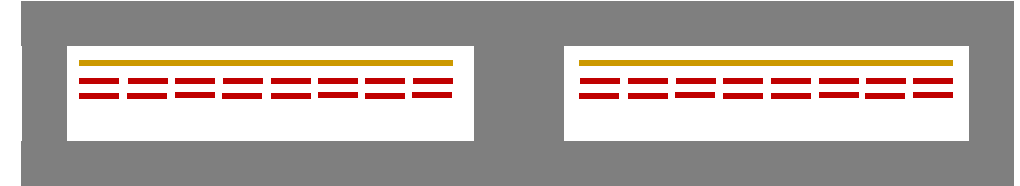


Minimizing Turns Count is Greatly Advantageous

32:2

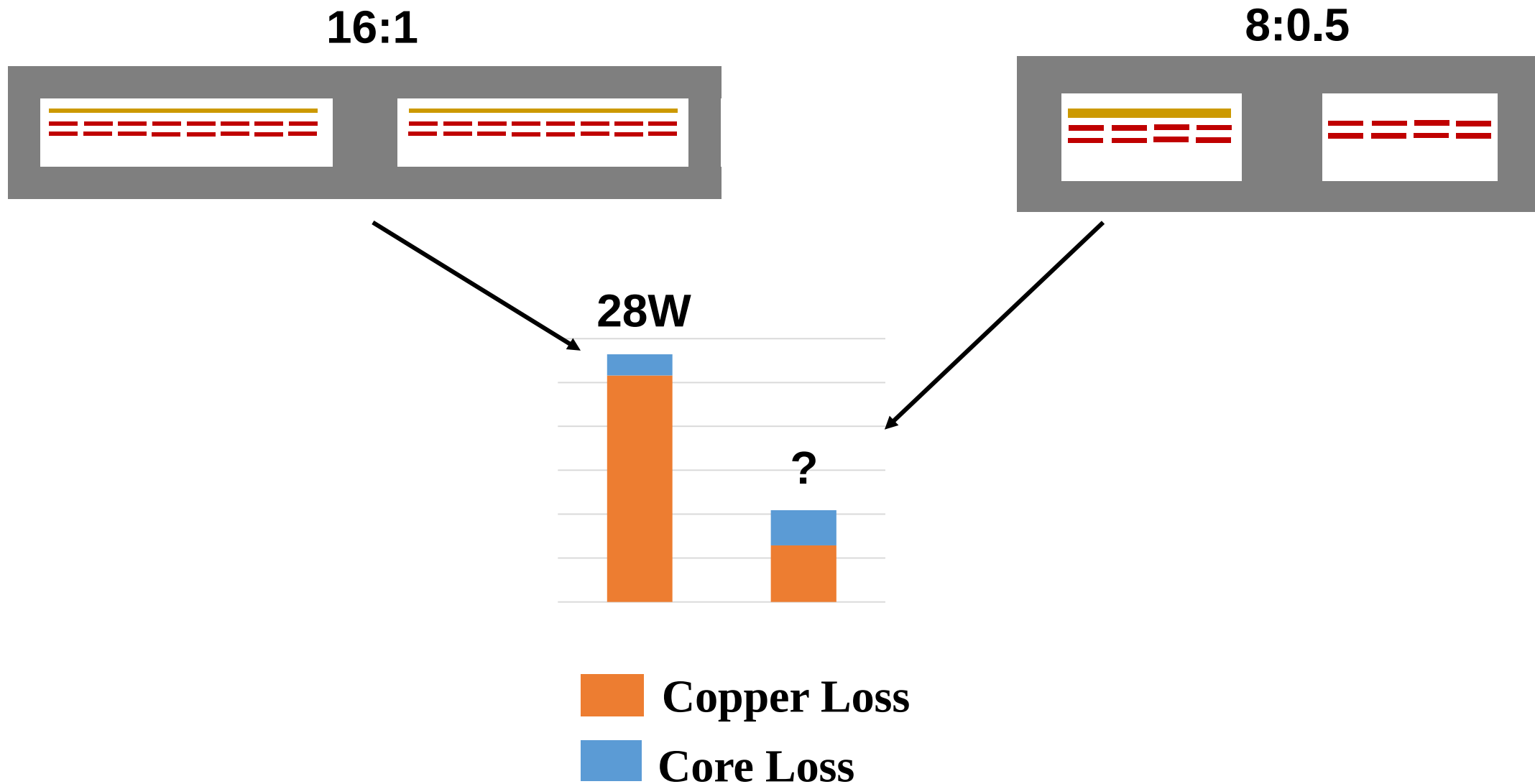


16:1

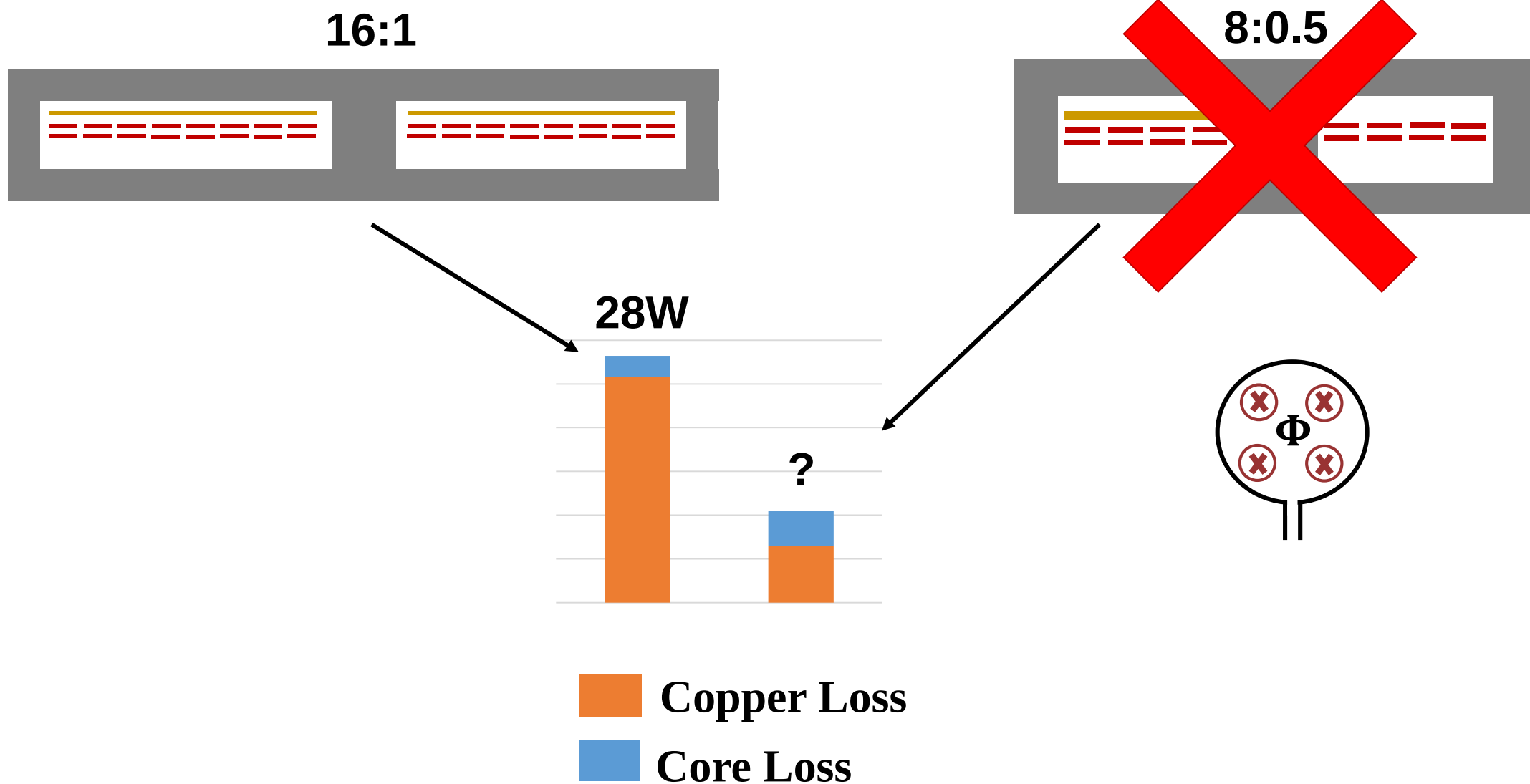


 Copper Loss
 Core Loss

A Fractional Turn is What We Want...

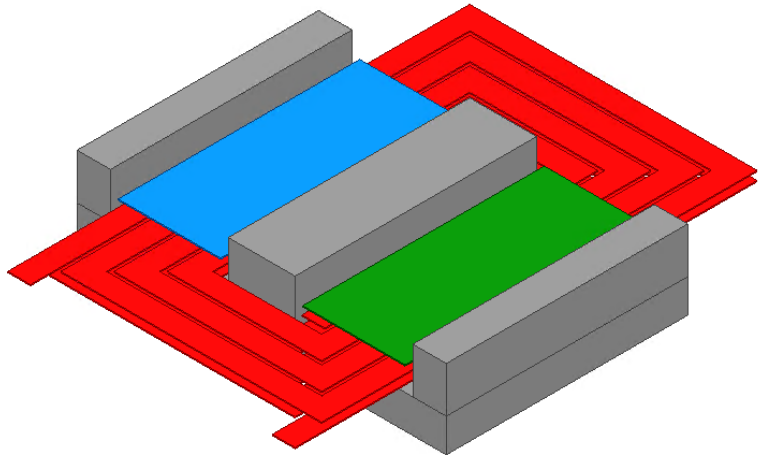


A Fractional Turn is What We Want... But Not Practical

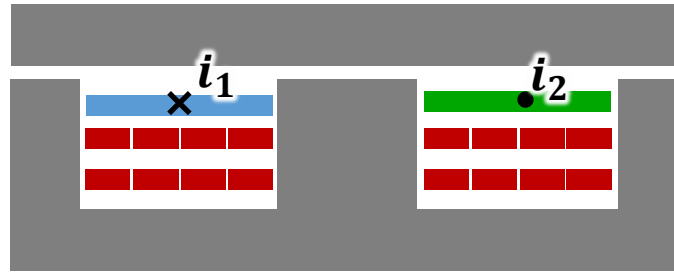


A Fractional-Turn Transformer Using a New Kind of Structure

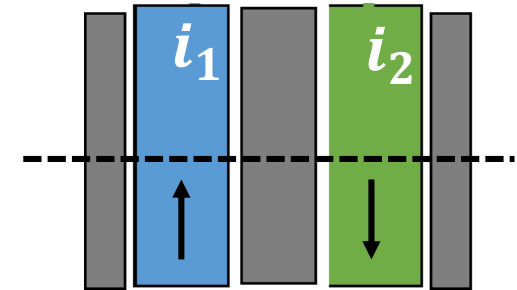
Orthographic View



Side View



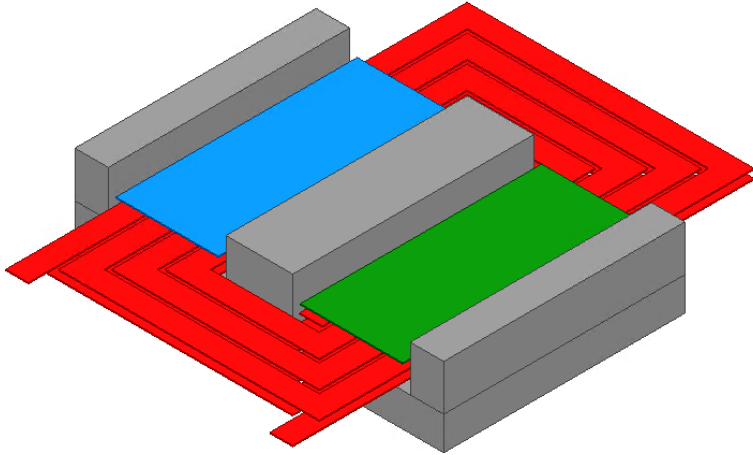
Top View



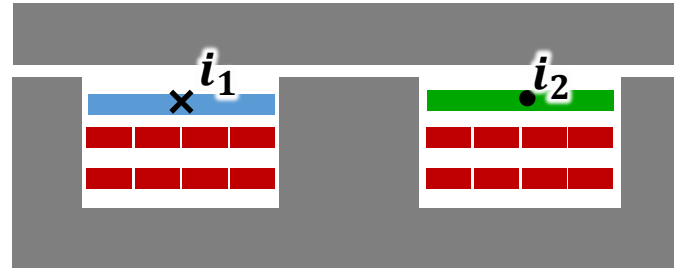
Assume Physical Symmetry About Center of the Core

Assume symmetry

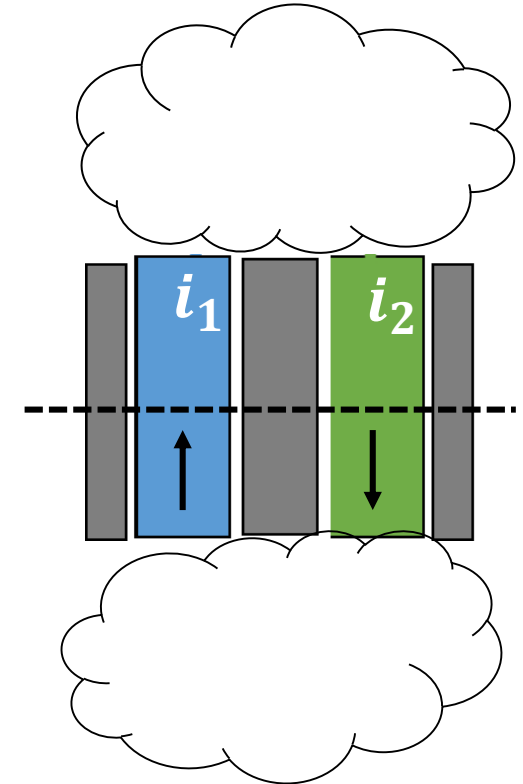
Orthographic View



Side View



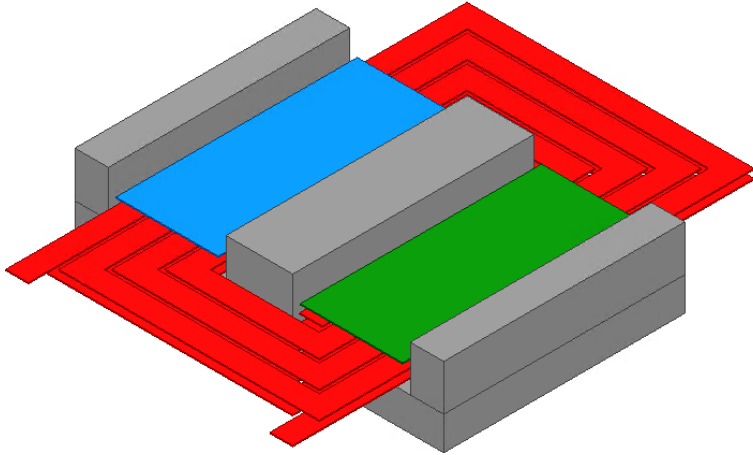
Top View



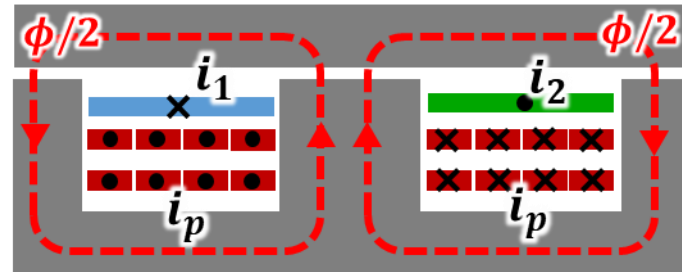
Excite the Primary Winding, Flux Flows Symmetrically

Assume symmetry

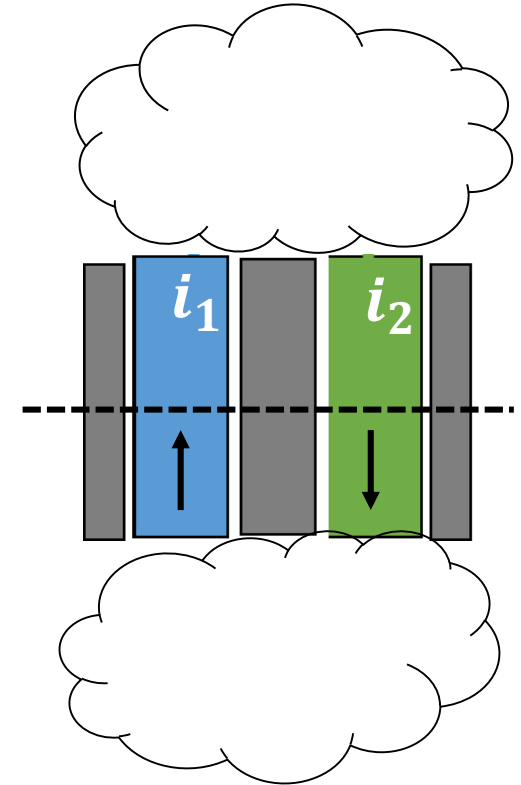
Orthographic View



Side View



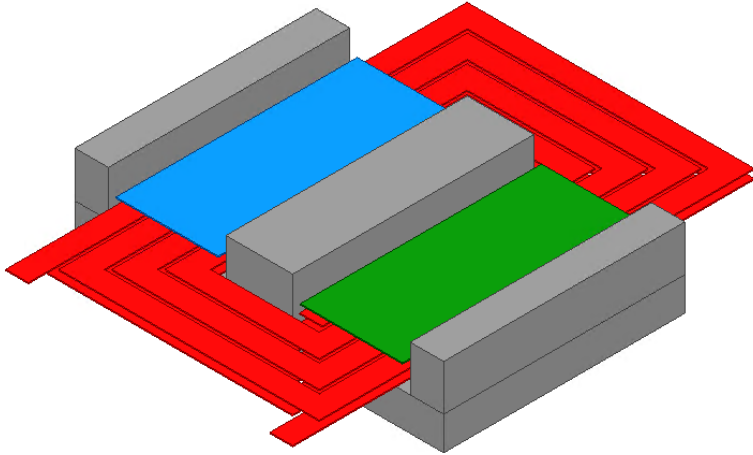
Top View



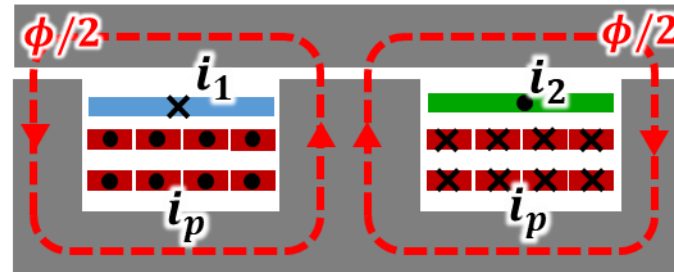
Symmetry and Magnetic Core Enforce Equal Currents

Assume symmetry

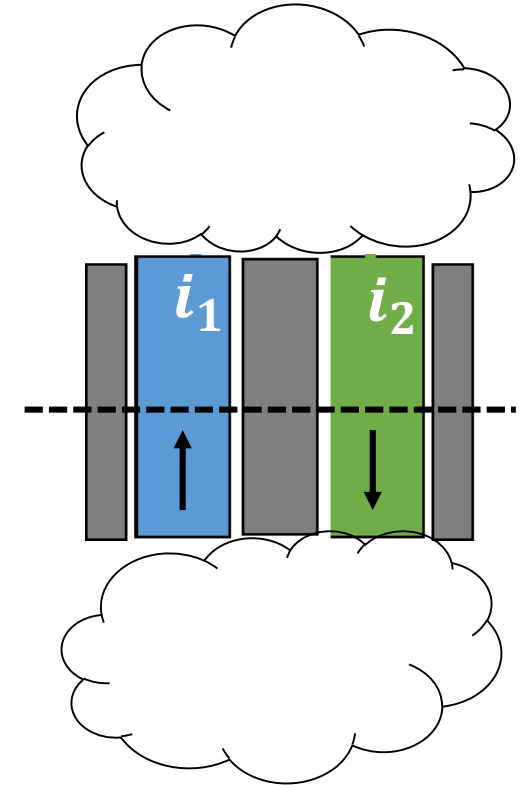
Orthographic View



Side View



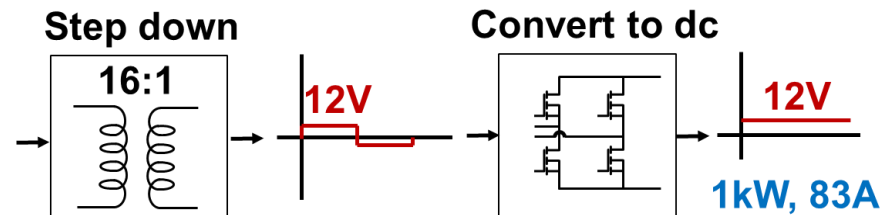
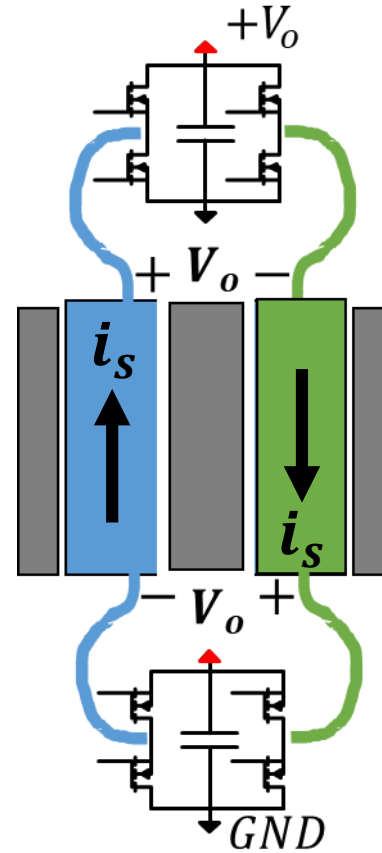
Top View



$$\oint H \cdot dl = 8i_p - i_1 = 8i_p - i_2 \quad \Rightarrow \quad i_1 = i_2 \text{ by } \underline{\text{symmetry}}$$

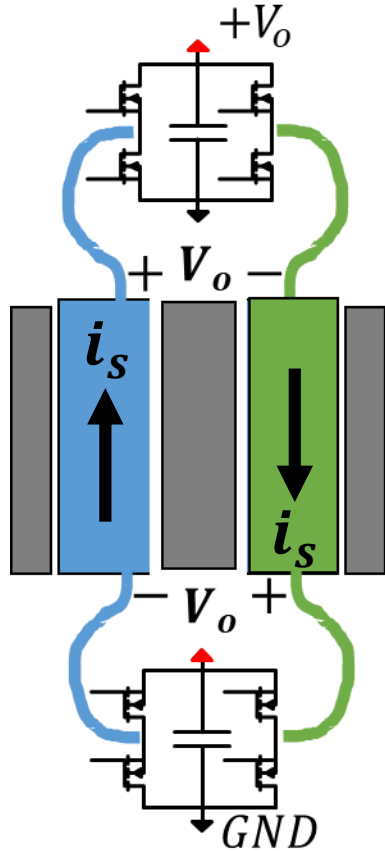
Symmetrically Distribute Two Full Bridge Rectifiers Around the Core

Top View



The Structure Behaves Like a Fractional Turn Transformer

Top View

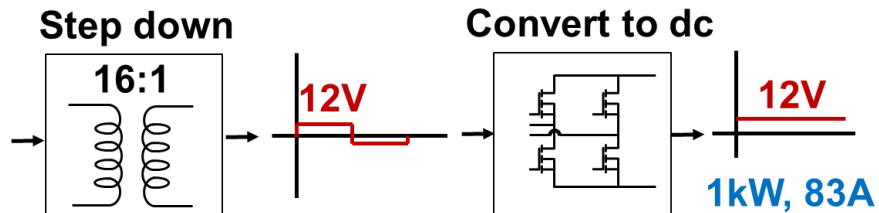


- Free to treat conductors as independent elements
- Connections yield:

$$2V_o = \frac{V_p}{N_p}$$

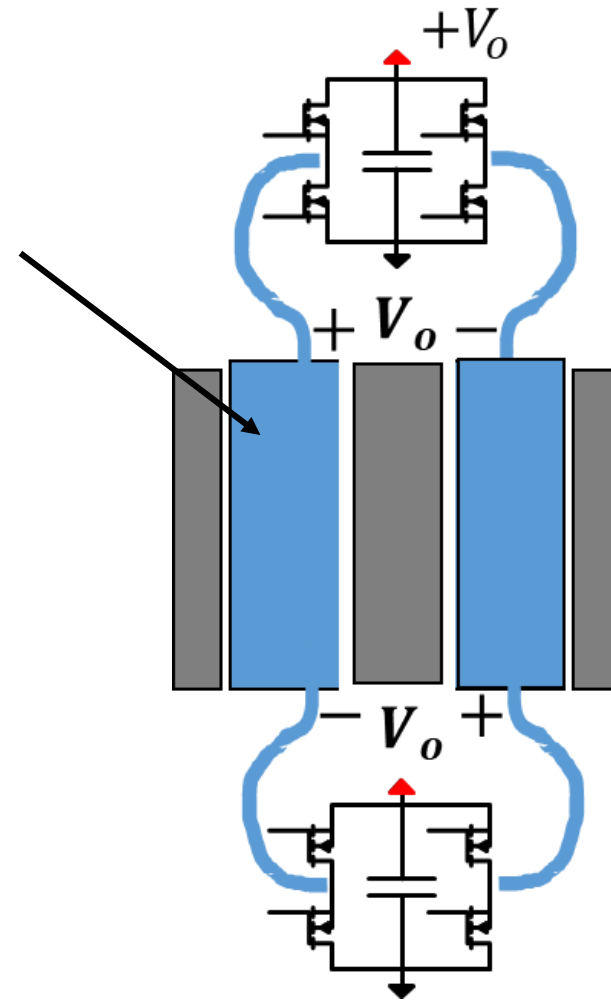
$$\frac{V_o}{V_p} = \frac{1/2}{N_p}$$

A **fractional turn** transformer



VIRT: An Example of a Coupled Electronic and Magnetic System

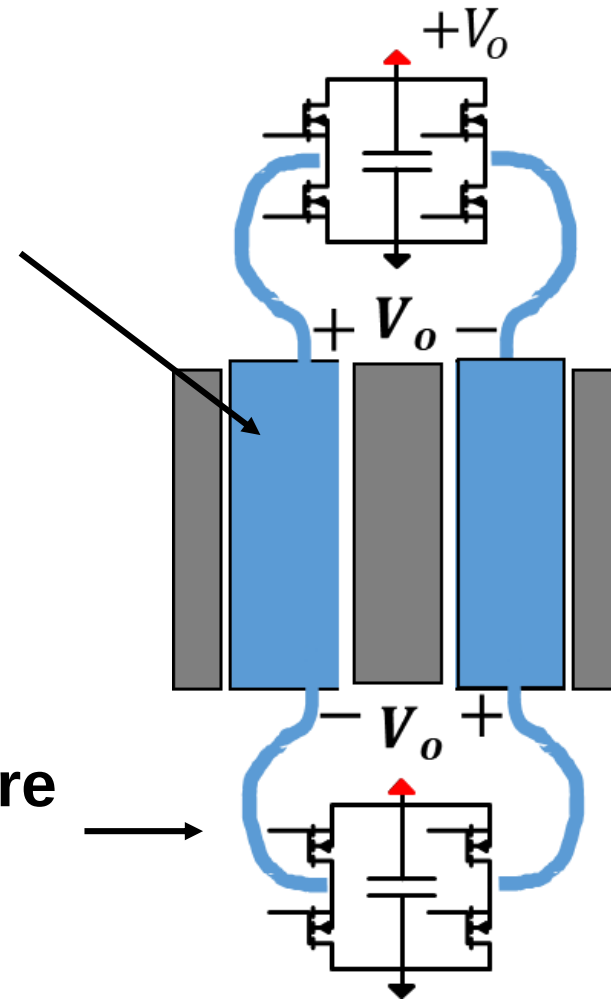
Equivalence of induced currents is ensured by symmetry



VIRT: An Example of a Coupled Electronic and Magnetic System

Equivalence of induced currents is ensured by symmetry

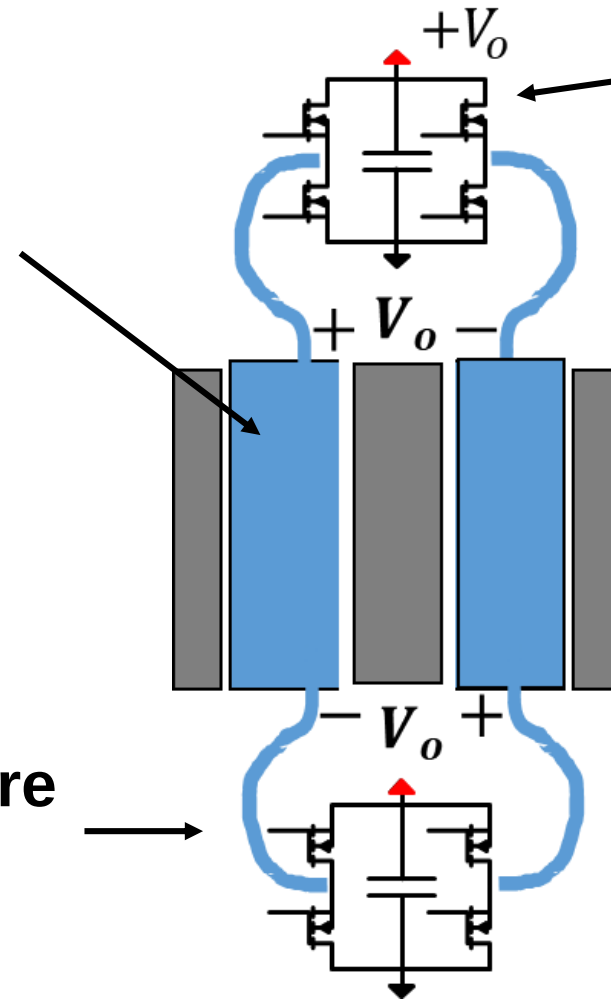
Connecting electronics are physically distributed around the core



VIRT: An Example of a Coupled Electronic and Magnetic System

Equivalence of induced currents is ensured by symmetry

Connecting electronics are physically distributed around the core



Electronics can be controlled to modify magnetic properties

FB/FB: $N_p: \frac{1}{2}$

FB/HB: $N_p: \frac{2}{3}$

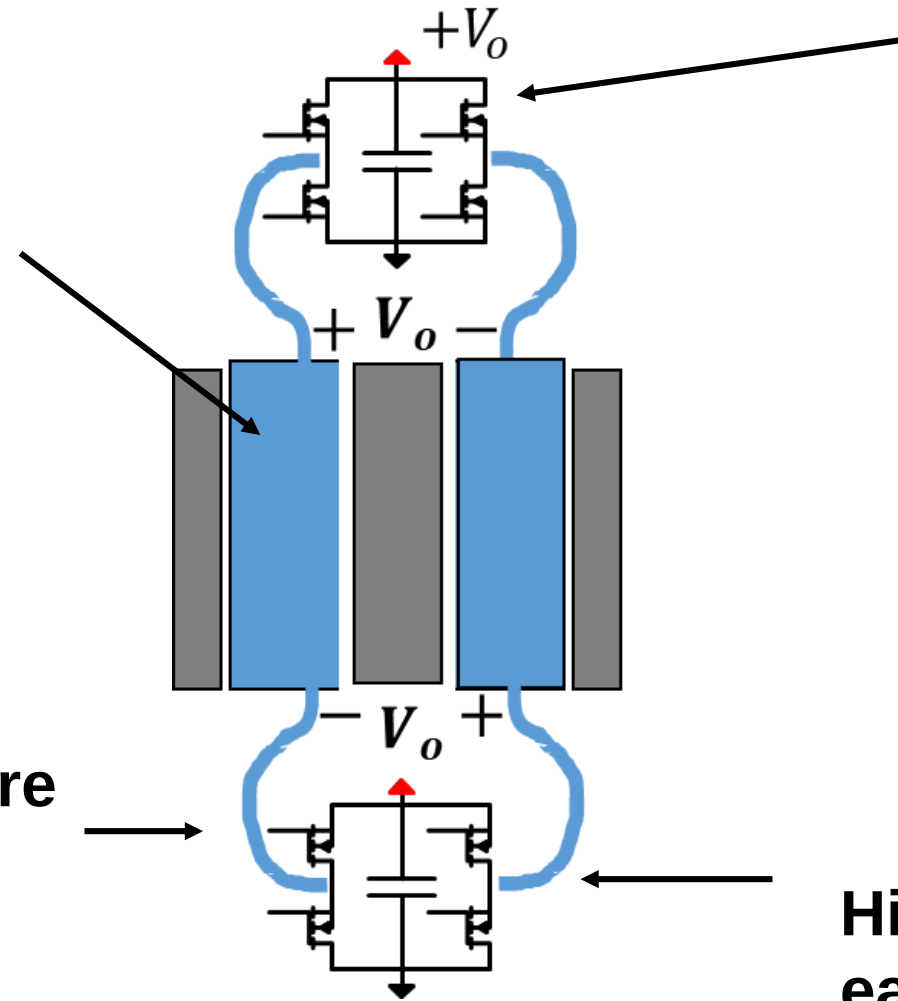
HB/HB: $N_p: 1$

HB/0: $N_p: 2$

VIRT: An Example of a Coupled Electronic and Magnetic System

Equivalence of induced currents is ensured by symmetry

Connecting electronics are physically distributed around the core



Electronics can be controlled to modify magnetic properties

$$\text{FB/FB: } N_p: \frac{1}{2}$$

$$\text{FB/HB: } N_p: \frac{2}{3}$$

$$\text{HB/HB: } N_p: 1$$

$$\text{HB/0: } N_p: 2$$

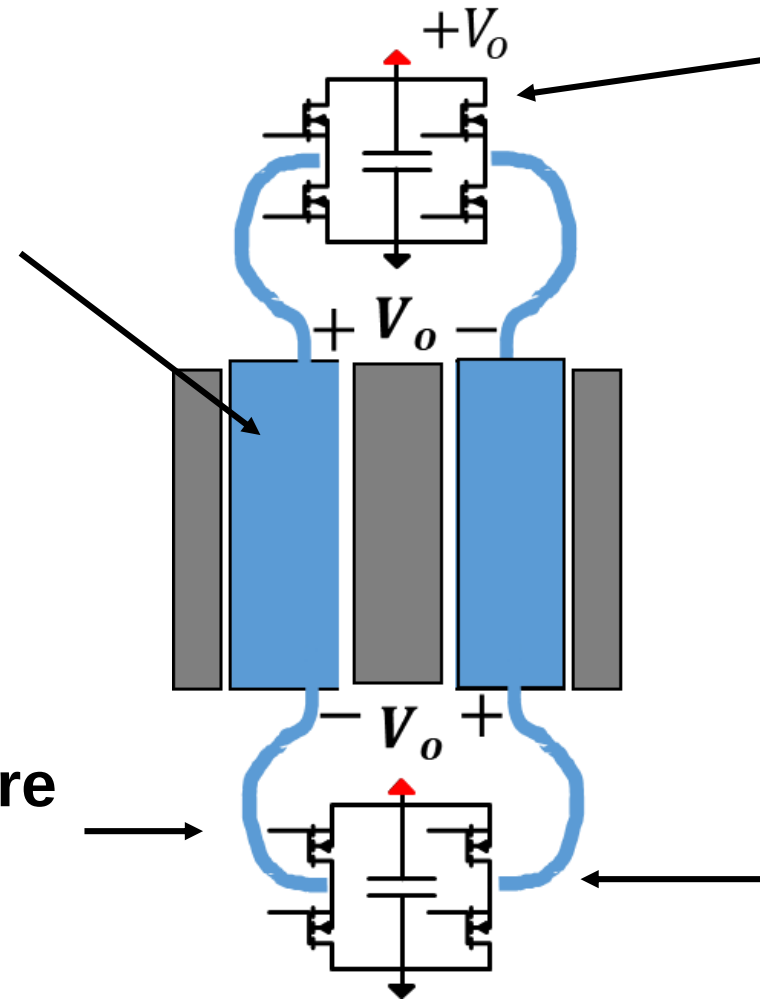
Higher switch count, but each carries less current (effectively paralleled)

VIRT: An Example of a Coupled Electronic and Magnetic System

Equivalence of induced currents is ensured by symmetry

Connecting electronics are physically distributed around the core

Requires a different modeling framework



Electronics can be controlled to modify magnetic properties

$$\text{FB/FB: } N_p: \frac{1}{2}$$

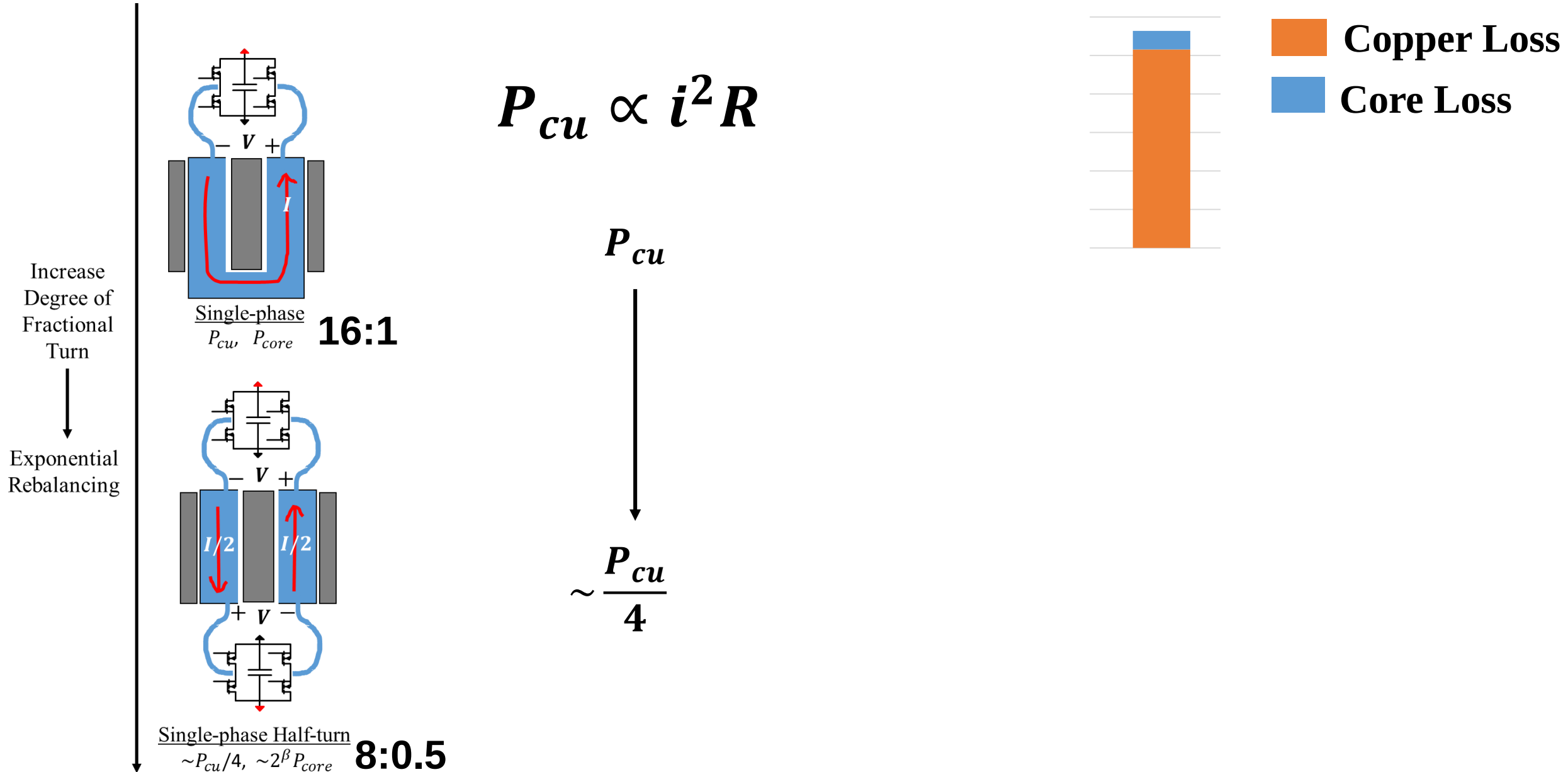
$$\text{FB/HB: } N_p: \frac{2}{3}$$

$$\text{HB/HB: } N_p: 1$$

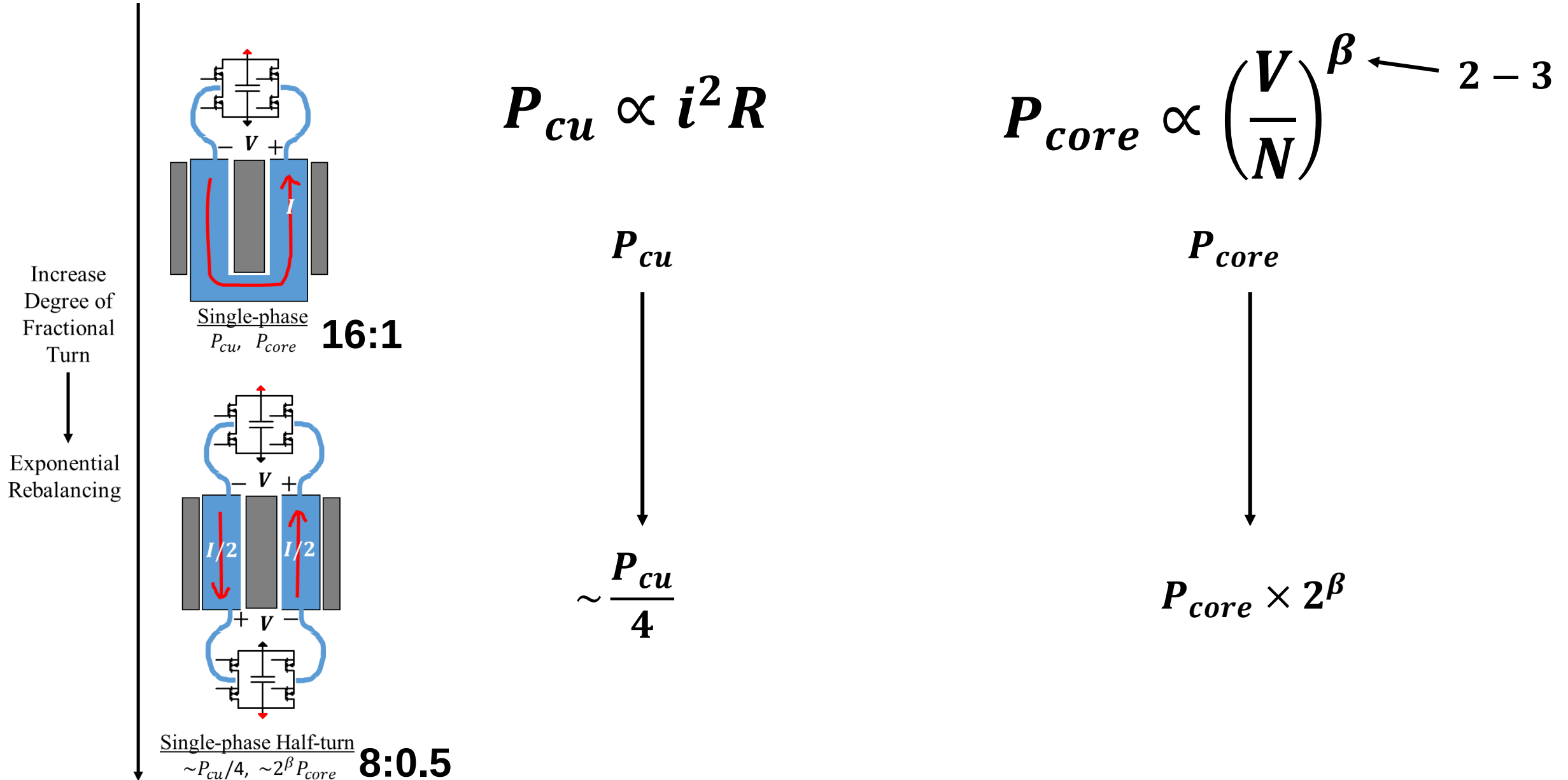
$$\text{HB/0: } N_p: 2$$

Higher switch count, but each carries less current (effectively paralleled)

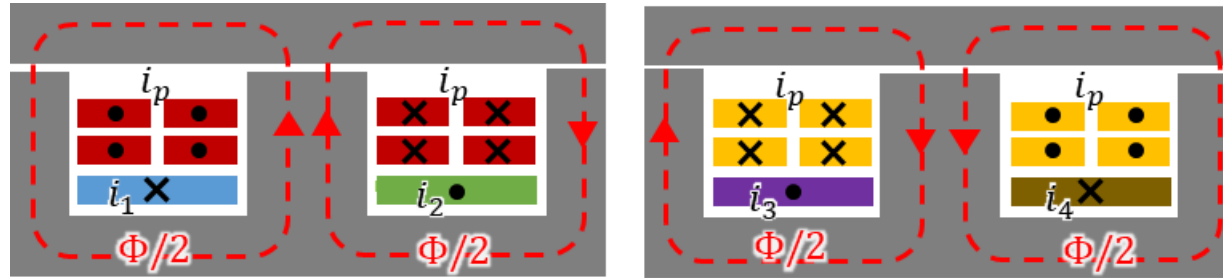
VIRT Exponentially Reduces Copper Loss



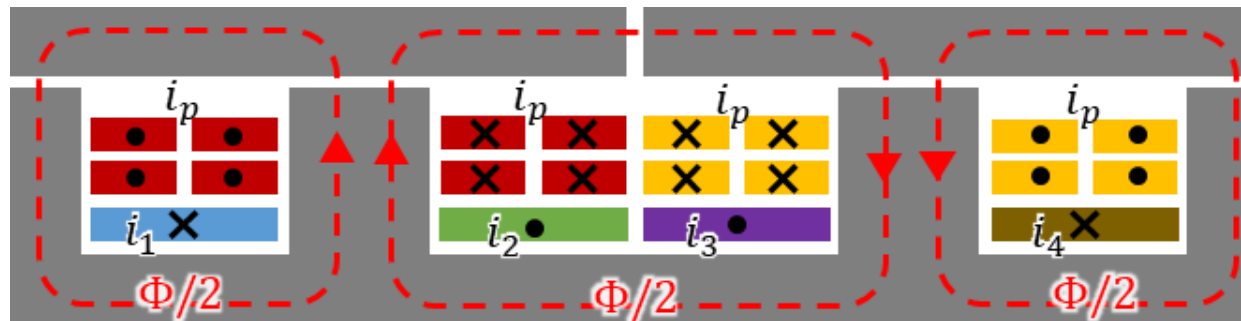
VIRT Exponentially Reduces Copper Loss and Increases Core Loss



The Conventional Approach: Increasing Phase Count



Combine

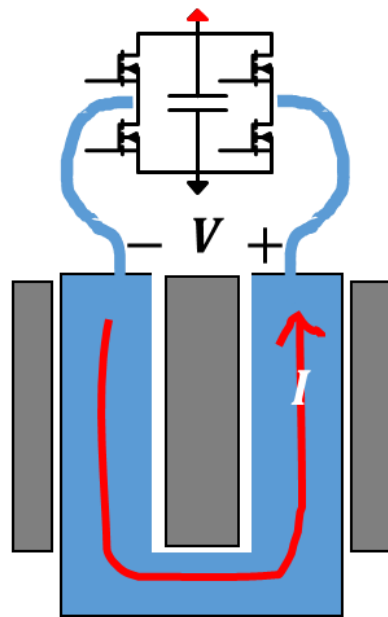


Wound such that equal and opposite flux flows on outer legs

Combine cores for volume reduction

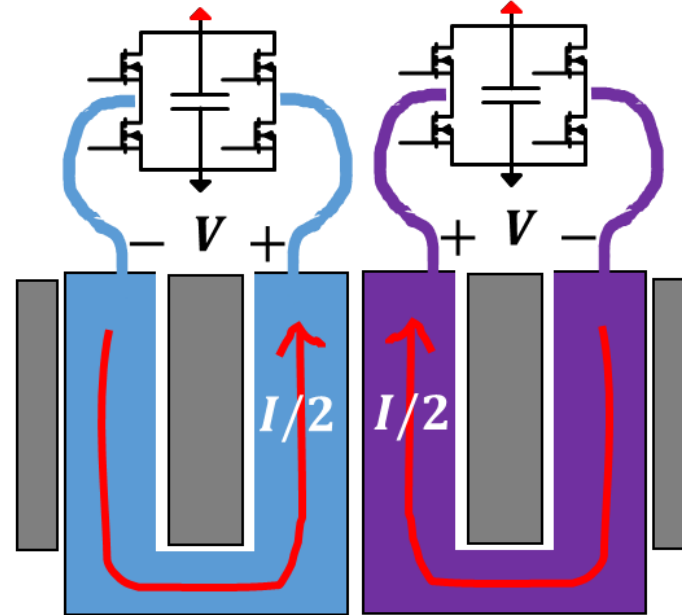
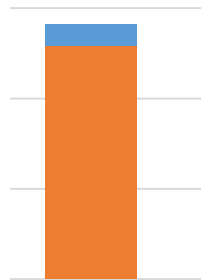
Increasing Phase Count Yields Linear Rebalancing

Increase Phase Count $\longrightarrow$ Linear Rebalancing



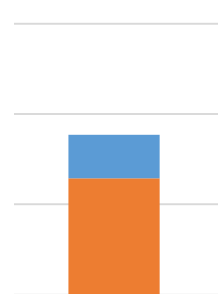
Single-phase

P_{cu} , P_{core}

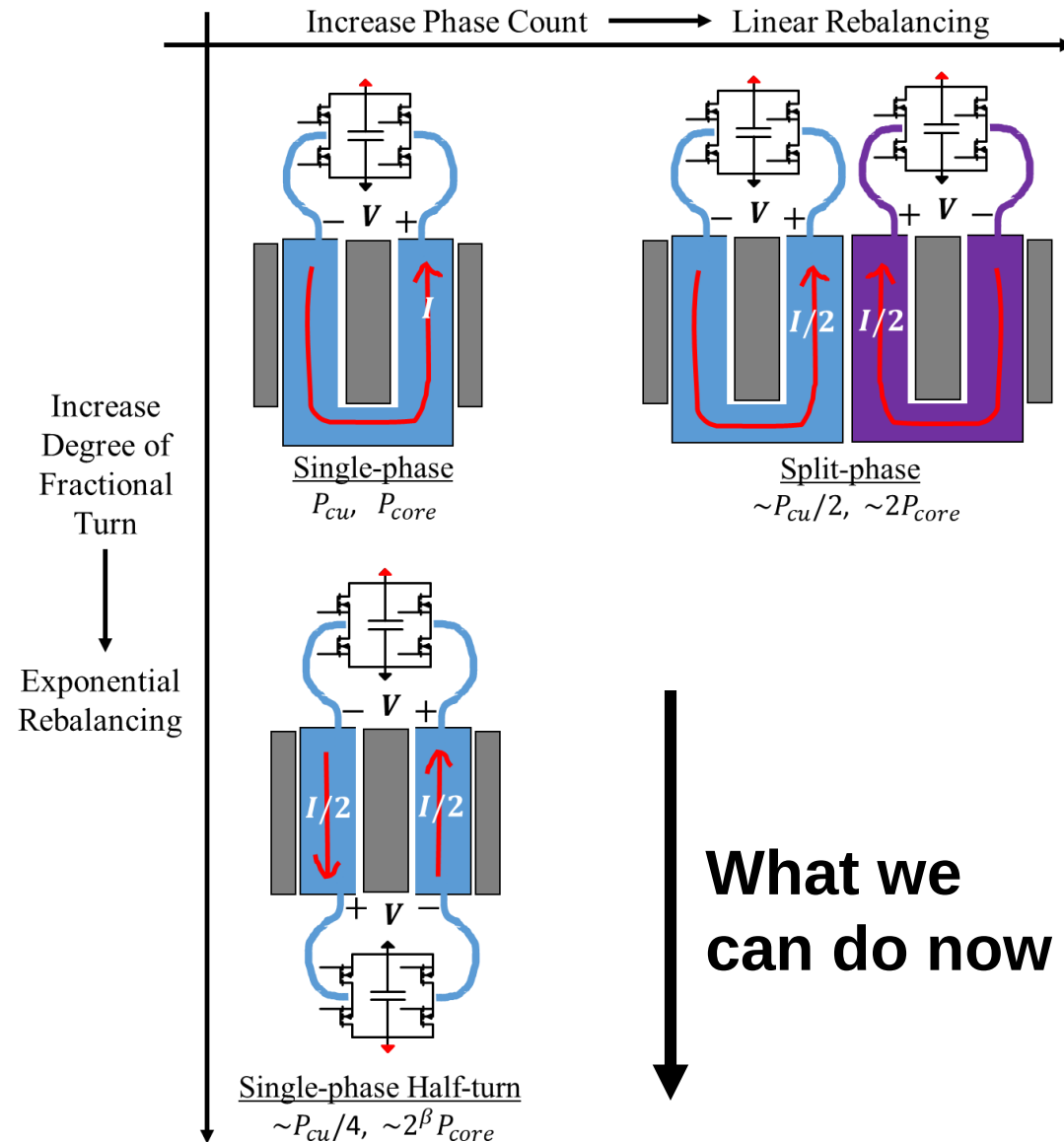


Split-phase

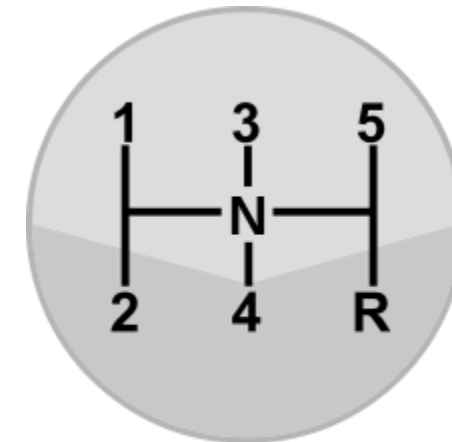
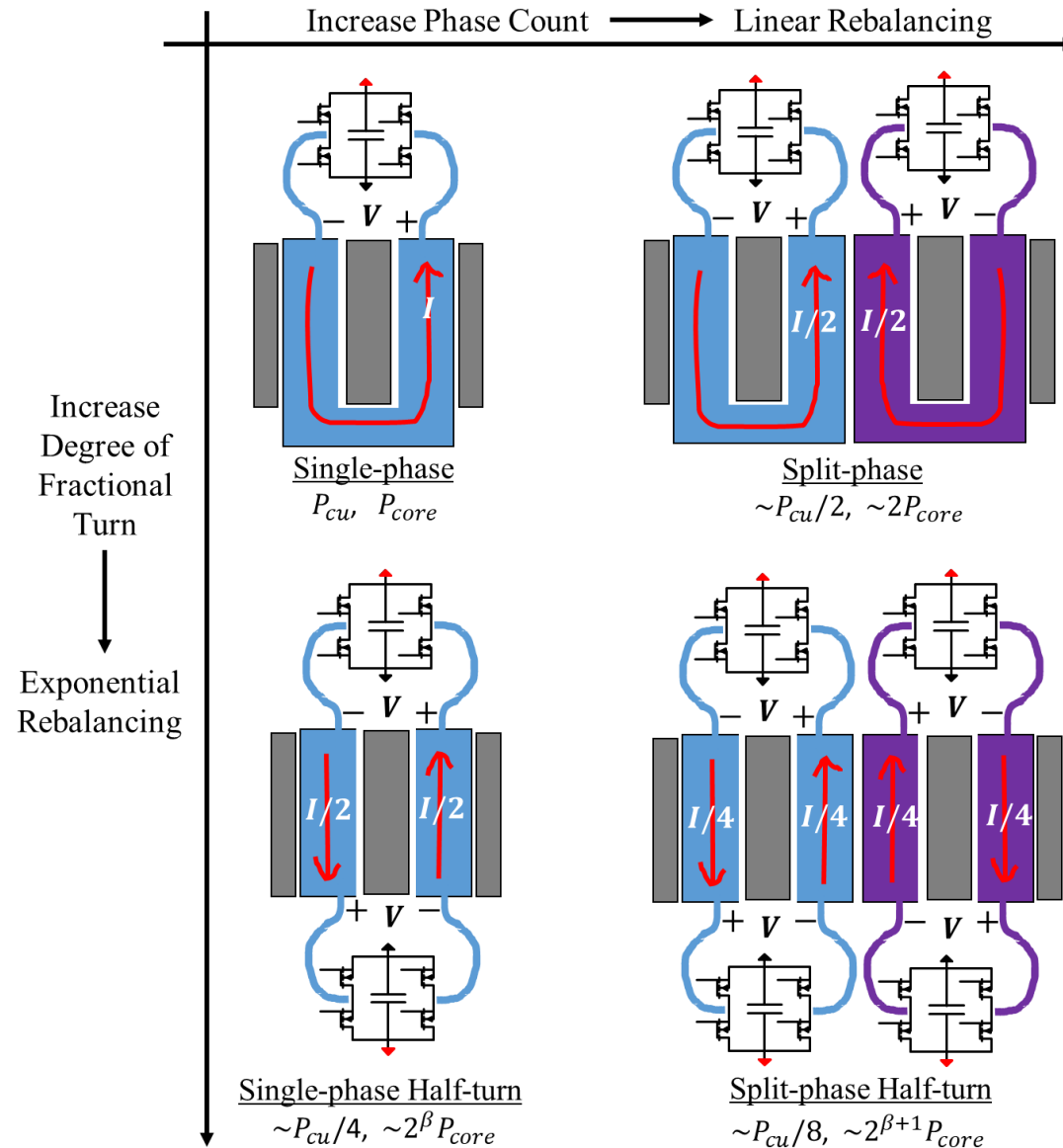
$\sim P_{cu}/2$, $\sim 2P_{core}$



These Techniques Offer Distinct Loss Trade-offs



“Gear Shifting” Transformer Core and Copper Loss

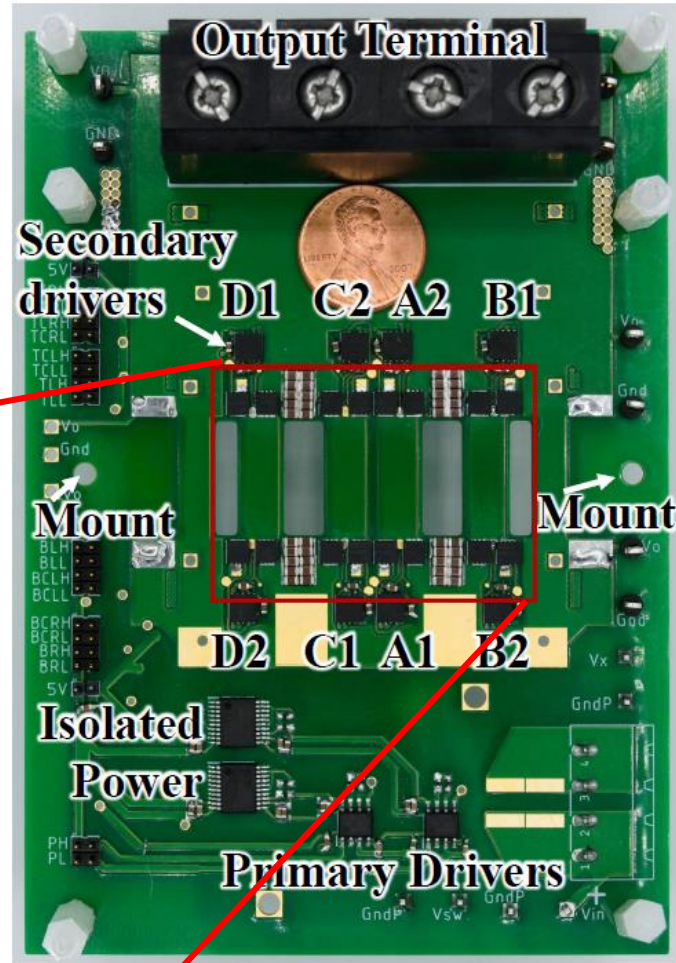
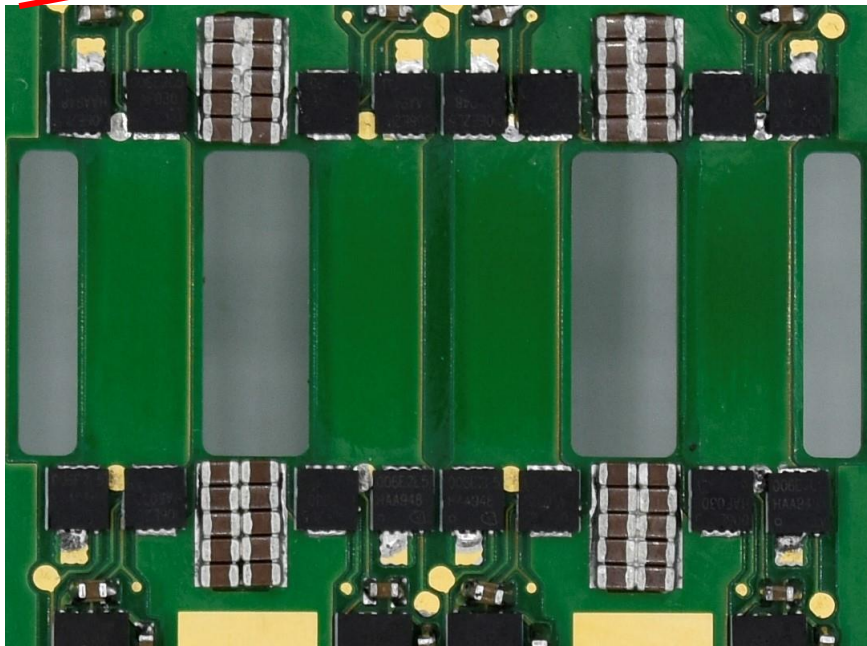


SPHTV

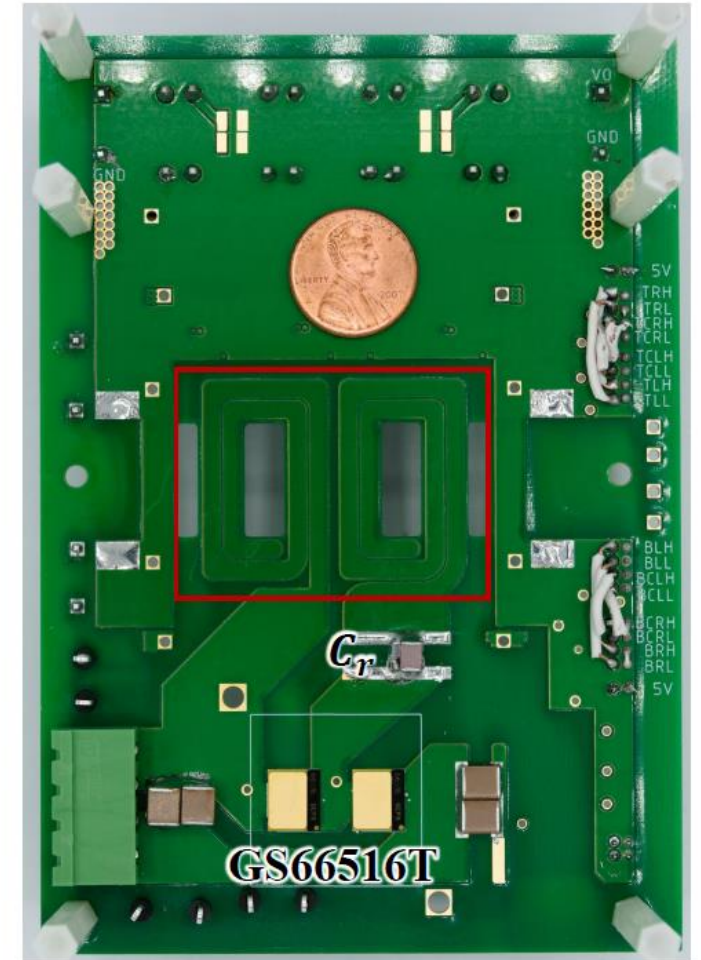
SPHTV Prototype



(a)



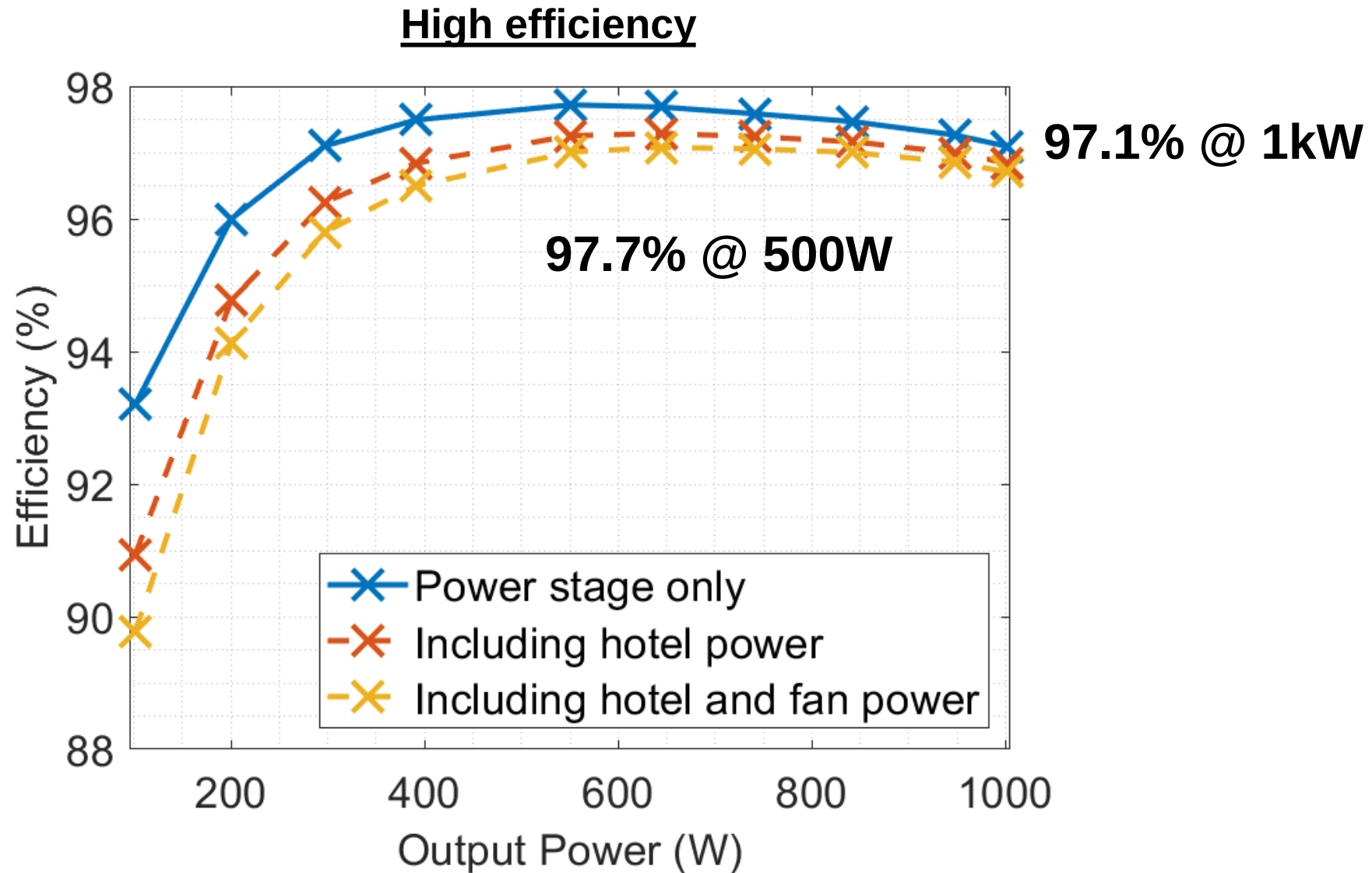
(c)



(d)

■ 4 layer, non-interleaved SPP, 3/2/3oz

Prototype is Extremely Efficient



Losses and Thermal Performance Well Predicted

Losses fit expectation

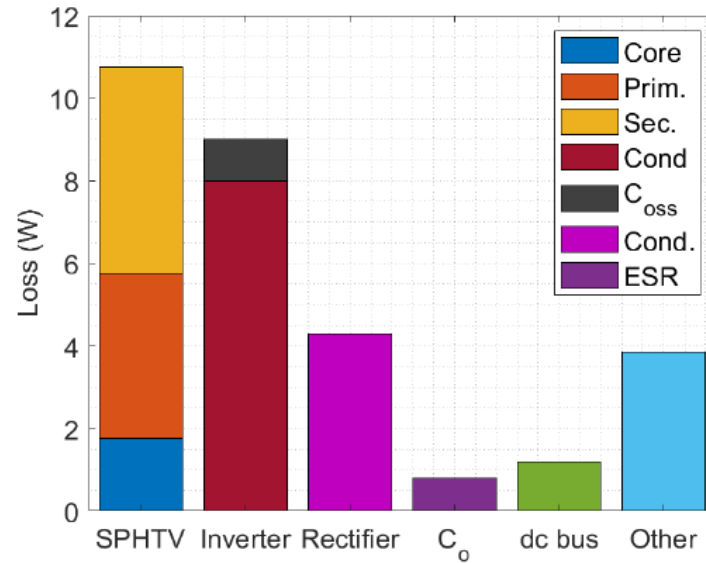


Fig. 12: Estimated loss breakdown at full load, not including hotel power (2.7W) and fan power (1.44W).

Thermal performance

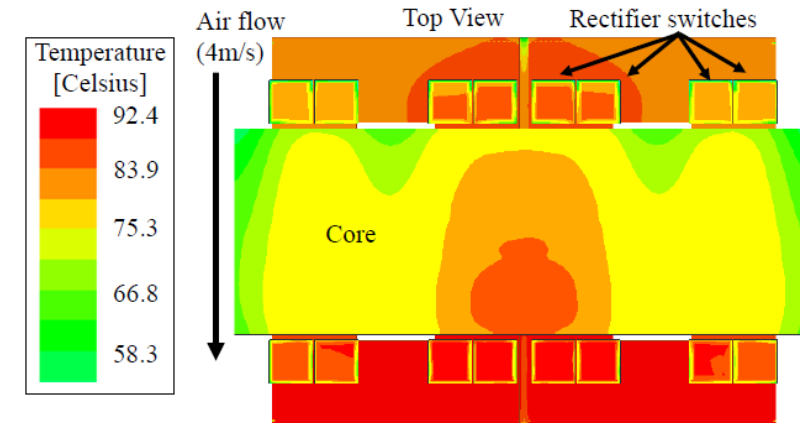


Fig. 7: ANSYS Icepak thermal simulation of the transformer.

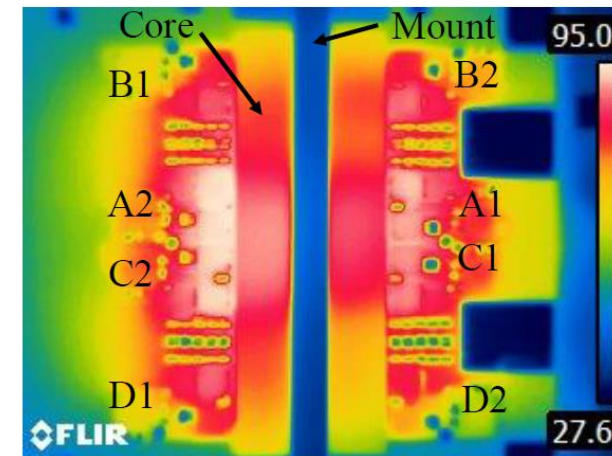


Fig. 11: Thermal image of secondary-side under full-load (obtained after 15 minutes of continuous operation, 22°C room temperature). The fan is located to the right of the PCB.

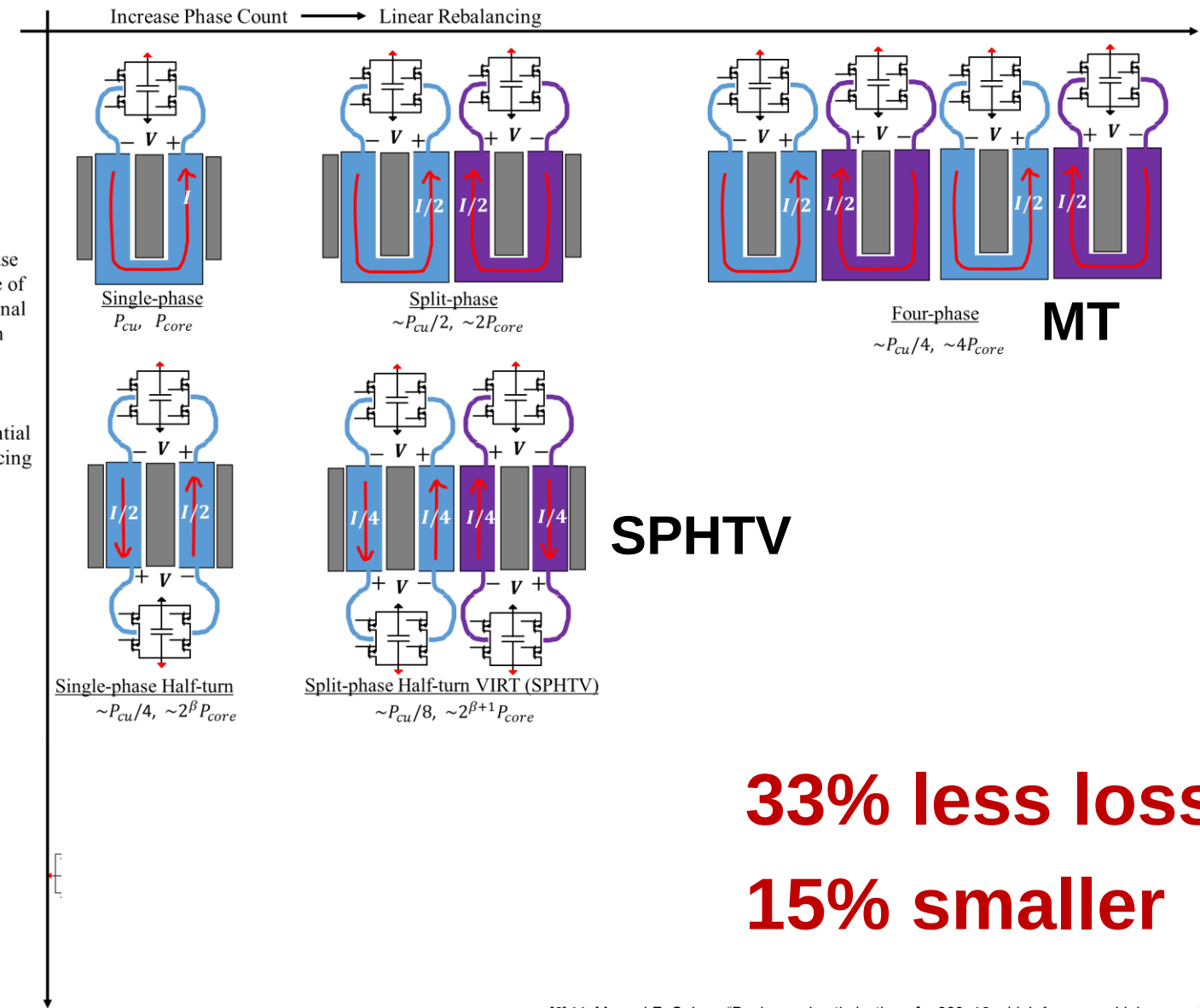
SPHTV: Much Lower Loss and Much Smaller than Best Alternatives

380-12V, 1kW

	This work	MT [6]
Stack-up	S/_P/P	S/P/P/S
Peak power stage efficiency	97.7%	-
Peak efficiency including hotel power	97.3%	97.1%
Full load loss (power stage only) [W]	29.9	34.4
Transformer loss at full load [W]	10.8	16.3
Transformer footprint [mm ²]	1536	2200
Height [mm]	9.23	7.3
Transformer box volume [cm ³]	14.2	16.1

^a 'G' is a secondary layer tied directly to secondary ground

33% less loss
15% smaller

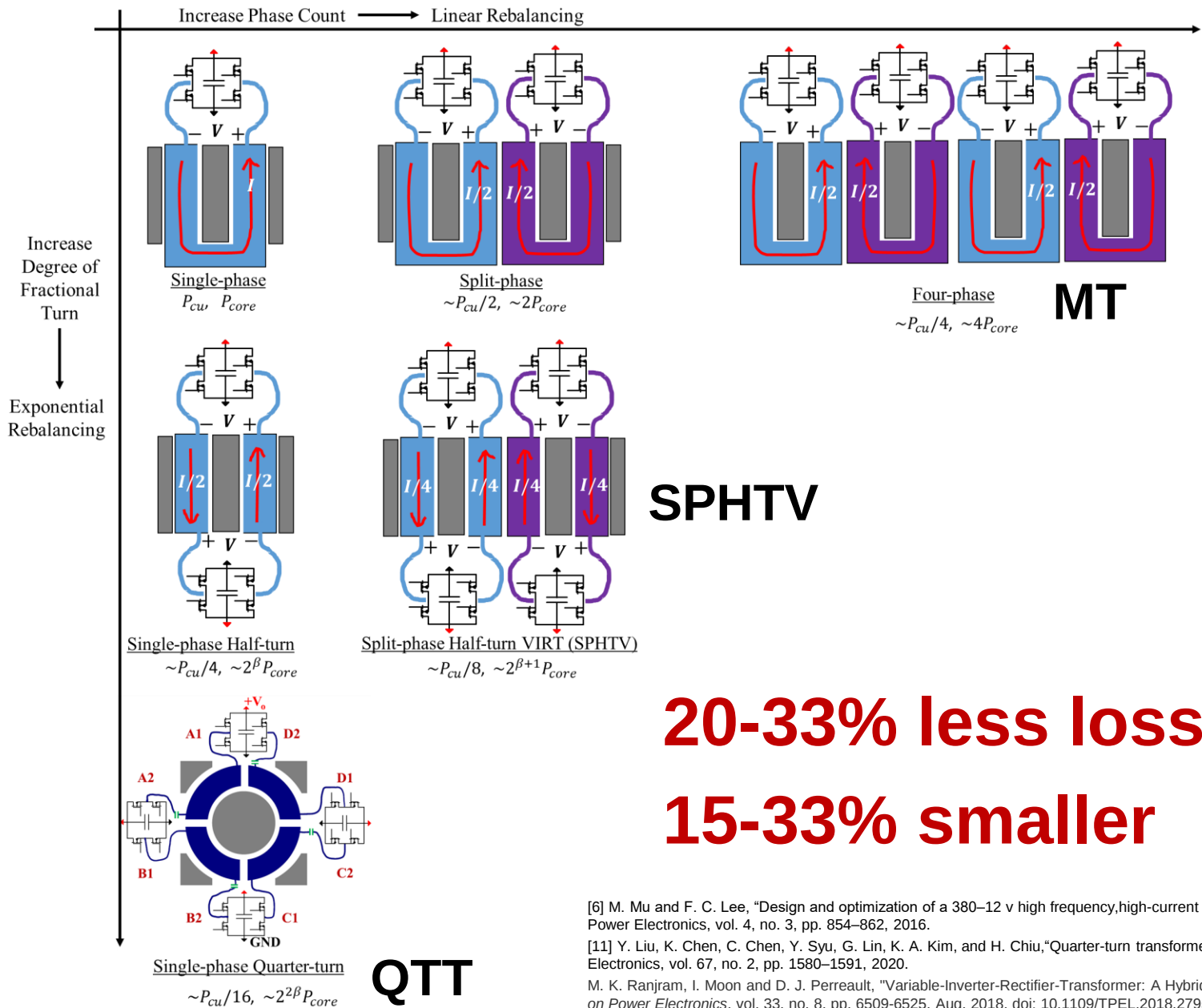


[6] M. Mu and F. C. Lee, "Design and optimization of a 380–12 v high frequency, high-current llc converter with gan devices and planar matrix transformers," IEEE Journal of Emerging and Selected Topics in Power Electronics, vol. 4, no. 3, pp. 854–862, 2016.

[11] Y. Liu, K. Chen, C. Chen, Y. Syu, G. Lin, K. A. Kim, and H. Chiu, "Quarter-turn transformer design and optimization for high power density 1-mhz llc resonant converter," IEEE Transactions on Industrial Electronics, vol. 67, no. 2, pp. 1580–1591, 2020.

SPHTV: Much Lower Loss and Much Smaller than Best Alternatives

380-12V, 1kW



20-33% less loss
15-33% smaller

	This work	MT [6]	QTT [11]
Stack-up	S/_/P/P	S/P/P/S	S/G/P/P/G/S ^a
Peak power stage efficiency	97.7%	-	97.0%
Peak efficiency including hotel power	97.3%	97.1%	-
Full load loss (power stage only) [W]	29.9	34.4	41
Transformer loss at full load [W]	10.8	16.3	13.2
Transformer footprint [mm ²]	1536	2200	2500
Height [mm]	9.23	7.3	8.9
Transformer box volume [cm ³]	14.2	16.1	22.3

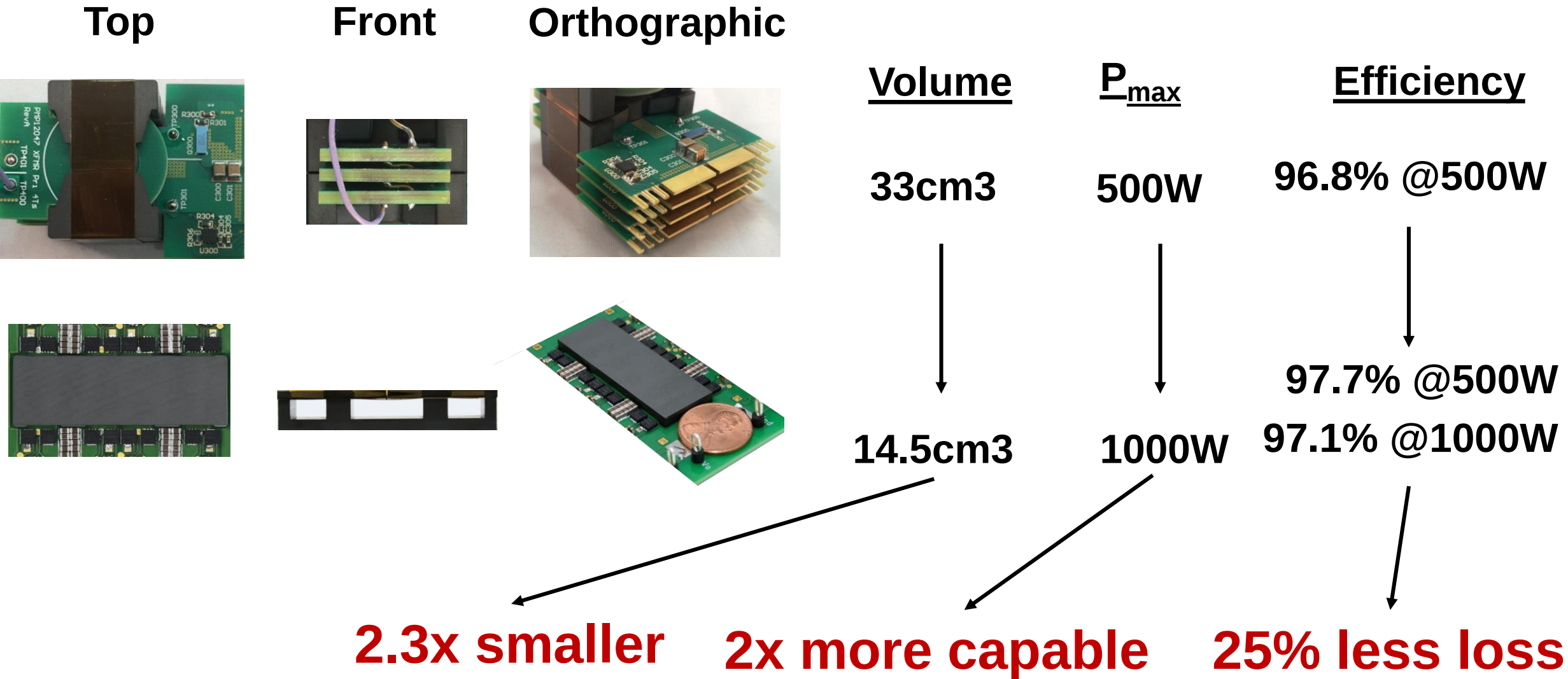
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[6] M. Mu and F. C. Lee, "Design and optimization of a 380–12 v high frequency, high-current llc converter with gan devices and planar matrix transformers," IEEE Journal of Emerging and Selected Topics in Power Electronics, vol. 4, no. 3, pp. 854–862, 2016.

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M. K. Ranjram, I. Moon and D. J. Perreault, "Variable-Inverter-Rectifier-Transformer: A Hybrid Electronic and Magnetic Structure Enabling Adjustable High Step-Down Conversion Ratios," in IEEE Transactions on Power Electronics, vol. 33, no. 8, pp. 6509–6525, Aug. 2018, doi: 10.1109/TPEL.2018.2795959.

Much More Efficient, Capable, Smaller than Industry Reference Design



Conclusion

- Coupled Electronic and Magnetic System (CEMS) paradigm enables the VIRT concept
- Fractional and variable turns ratios unachievable in conventional design
- Used to build **much smaller and much more efficient** datacenter supply

